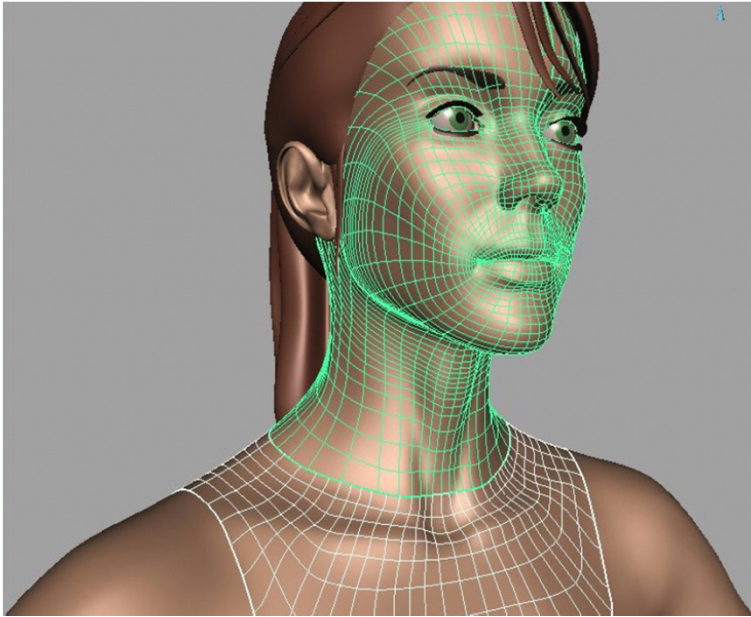
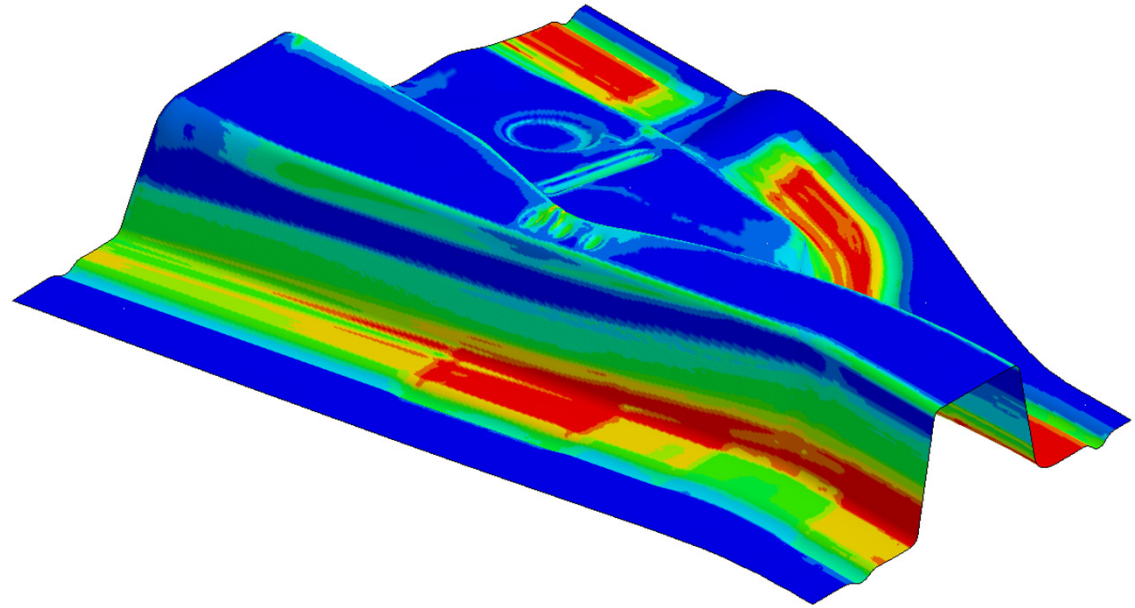


Recent developments in LS-DYNA for Isogeometric Analysis



T.J.R. Hughes



Stefan Hartmann

DYNAmore GmbH, Industriestr. 2, D-70565 Stuttgart, Germany

Some slides borrowed from:

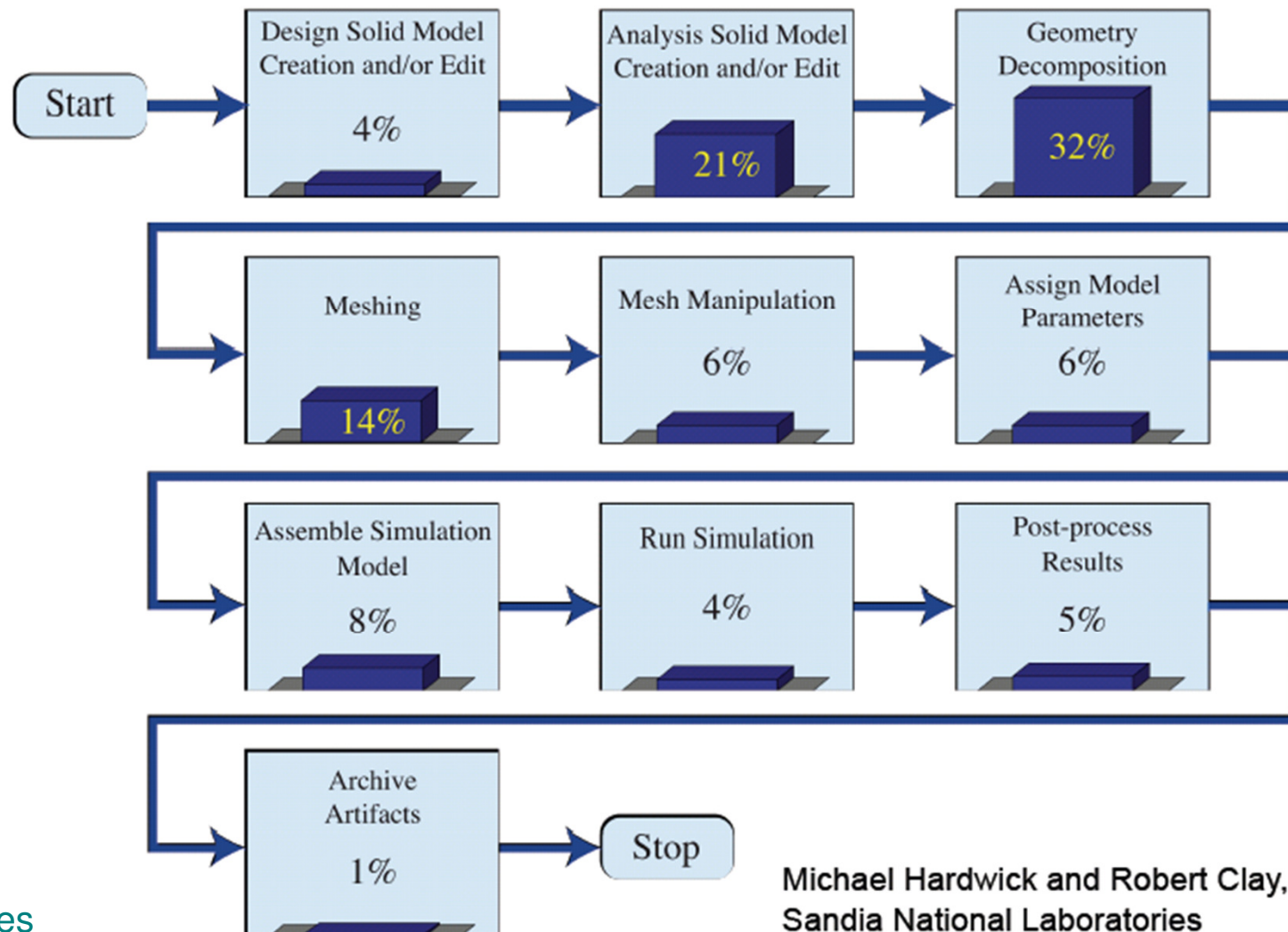
T.J.R. Hughes: Professor of Aerospace Engineering and Engineering Mechanics, University of Texas at Austin
D.J. Benson: Professor of Applied Mechanics, University of California, San Diego

Outline

- Isogeometric Analysis
 - motivation / definition / history
- From B-splines to NURBS (T.J.R. Hughes)
 - basis functions / control net / refinements
- *generalized elements* in LS-DYNA (D.J. Benson)
 - basic idea / shell formulations / interpolation-nodes / interpolation-elements
- NURBS-based finite elements in LS-DYNA
 - *ELEMENT_NURBS_PATCH_2D
- Example: Underbody Cross Member (Numisheet 2005)
 - description / comparison of results / summary
- Summary and Outlook

Isogeometric Analysis – motivation (... at the beginning)

- reduce effort of geometry conversion from CAD into a suitable mesh for FEA



T.J.R. Hughes

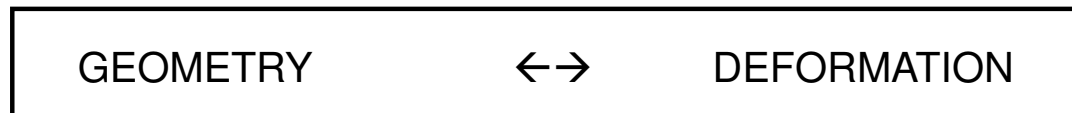
Michael Hardwick and Robert Clay,
Sandia National Laboratories

Isogeometric Analysis - definition

■ ISOPARAMETRIC (FE-Analysis)

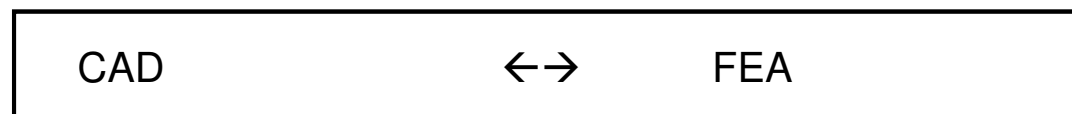
use same approximation for geometry and deformation

(normally: low order Lagrange polynomials ---- in LS-DYNA basically only linear elements)



■ ISOGEOMETRIC (CAD - FEA)

same description of the geometry in the design (CAD) and the analysis (FEA)



■ common geometry descriptions in CAD

- NURBS (Non-Uniform Rational B-splines) → most commonly used
- T-splines → enhancement of NURBS
- subdivision surfaces → mainly used in animation industry
- and others

Isogeometric Analysis - history

- start in 2003
 - summer: Austin Cotrell starts as PhD Student of Prof. T.J.R. Hughes at the University of Texas, Austin
 - autumn: first NURBS-based FE-code for linear, static problems provides promising results, the name „ISOGEOMETRIC“ is used the first time
- 2004 up to now: many research activities to various topics
 - non-linear structural mechanics
 - shells with and without rotational DOFs
 - implicit gradient enhanced damage
 - XFEM
 - shape- und topology-optimization
 - efficient numerical integration
 - turbulence and fluid-structure-interaction
 - acoustics
 - refinement strategies
 - ...
- January 2011: first thematic conference on *Isogeometric Analysis*
 - “Isogeometric Analysis 2011: Integrating Design and Analysis“, University of Texas at Austin

From B-splines to NURBS

■ B-spline basis functions

- constructed recursively
- positive everywhere (in contrast to Lagrange polynomials)
- shape of basis functions depend on: knot-vector and polynomial degree
- knot-vector: non-decreasing set of coordinates in parameter space
- normally $C^{(p-1)}$ -continuity

→ e.g. lin. / quad. / cub. / quart. Lagrange:

→ $C^0 / C^0 / C^0 / C^0$

→ e.g. lin. / quad. / cub. / quart. B-spline:

→ $C^0 / C^1 / C^2 / C^3$

Example of a uniform knot-vector:

$$\Xi = \{0, 1, 2, 3, 4, \dots\}$$

$p = 0$:

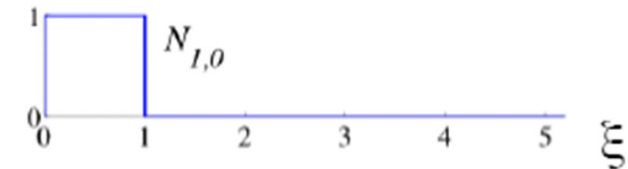
$$N_{i,0}(\xi) = \begin{cases} 1 & \text{if } \xi_i \leq \xi < \xi_{i+1} \\ 0 & \text{otherwise} \end{cases}$$

$p > 0$:

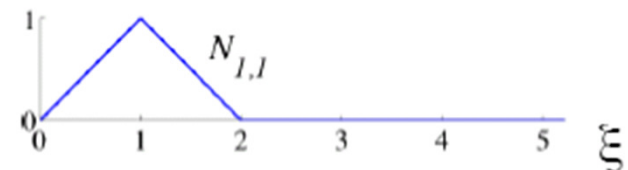
$$N_{i,p}(\xi) = \frac{\xi - \xi_i}{\xi_{i+p} - \xi_i} N_{i,p-1}(\xi) + \frac{\xi_{i+p+1} - \xi}{\xi_{i+p+1} - \xi_{i+1}} N_{i+1,p-1}(\xi)$$

T.J.R. Hughes

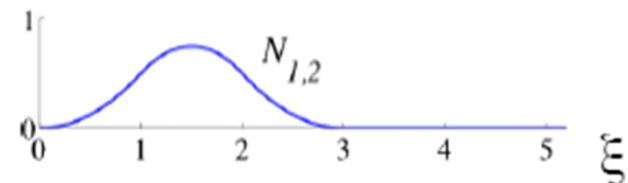
$p=0$



$p=1$



$p=2$



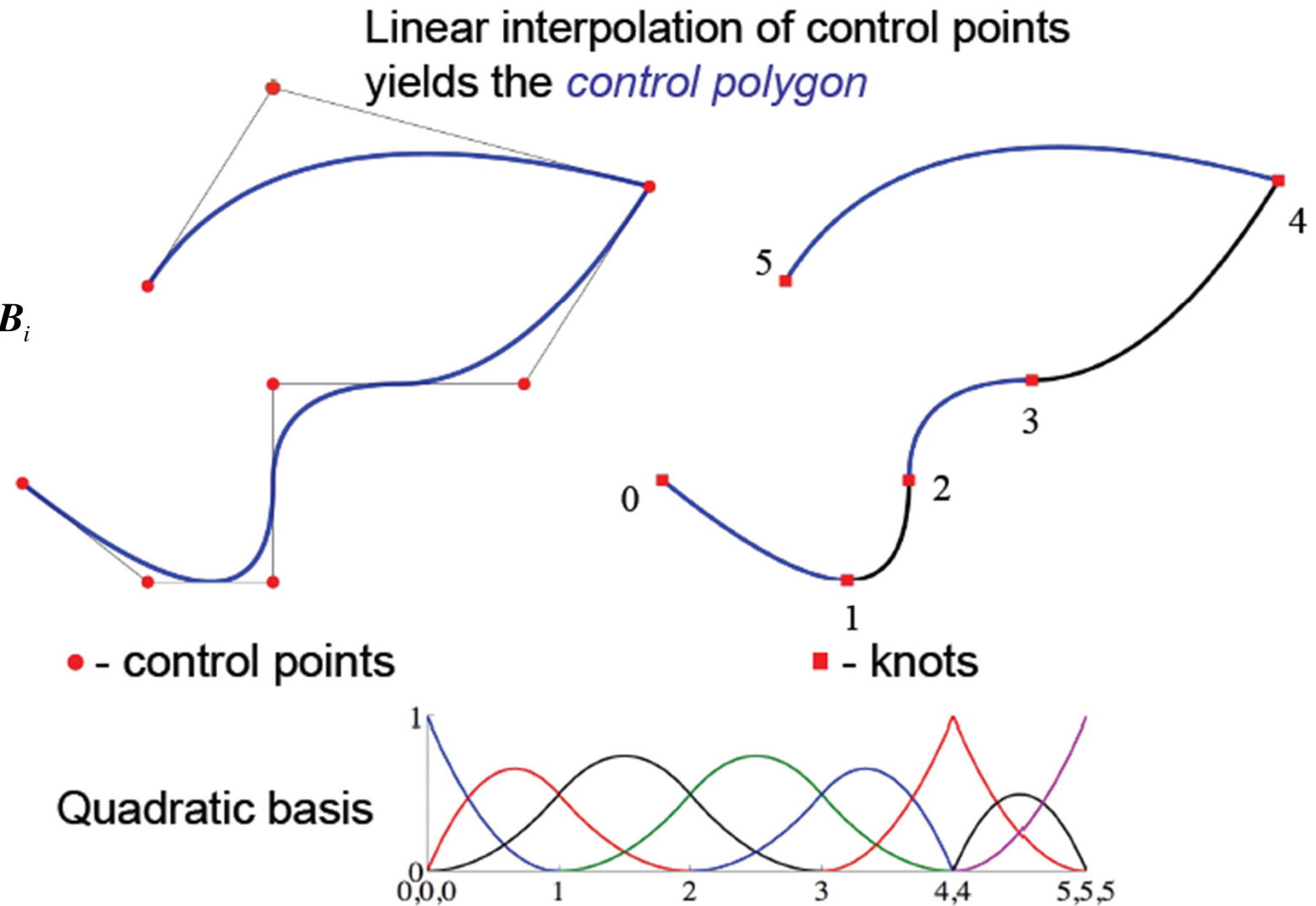
From B-splines to NURBS

■ B-spline curves

- control points \mathbf{B}_i / control polygon (control net)
- knots

linear combination:

$$\mathbf{C}(\xi) = \sum_{i=1}^n N_{i,p}(\xi) \mathbf{B}_i$$



T.J.R. Hughes

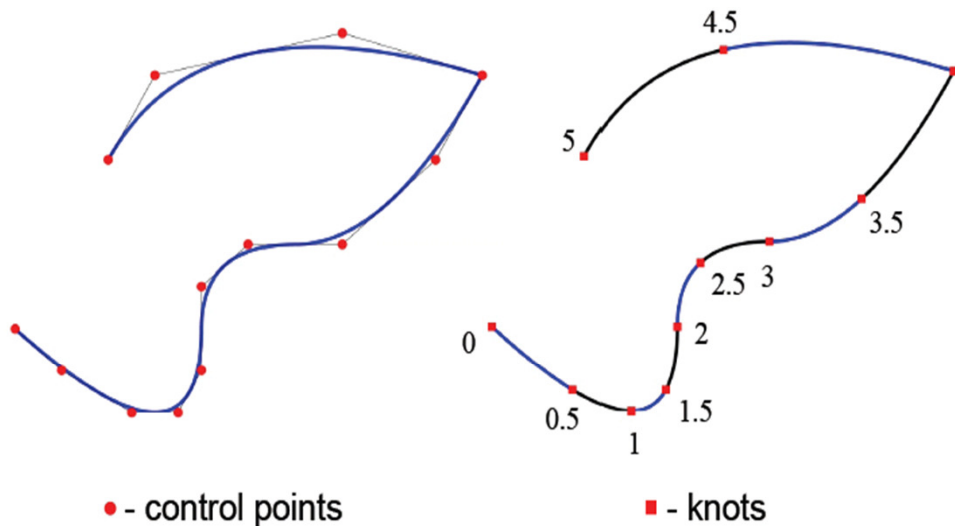
From B-splines to NURBS

■ B-splines

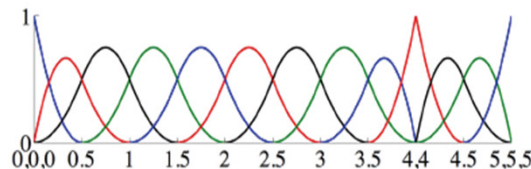
- refinement possibilities

h-refinement

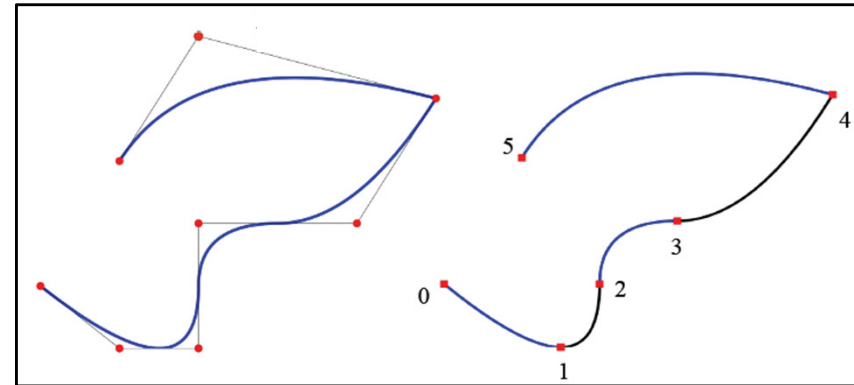
- number of elements increases
- order of polynomial remains the same



Quadratic basis

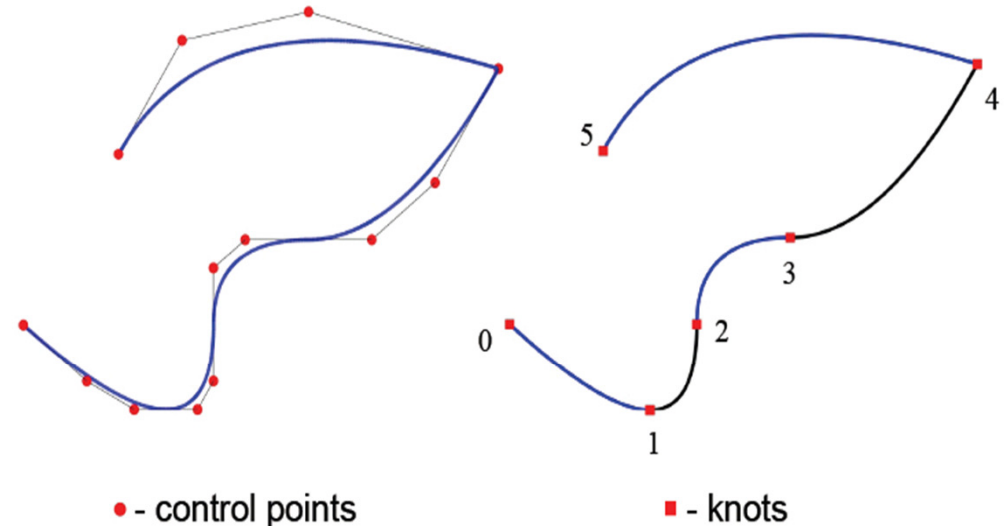


T.J.R. Hughes

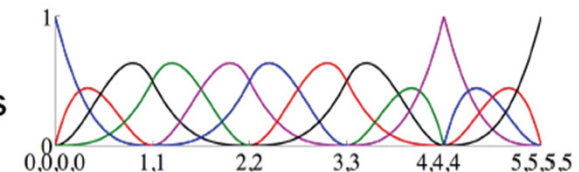


p-refinement

- number of elements remains the same
- order of polynomial increases



Cubic basis



From B-splines to NURBS

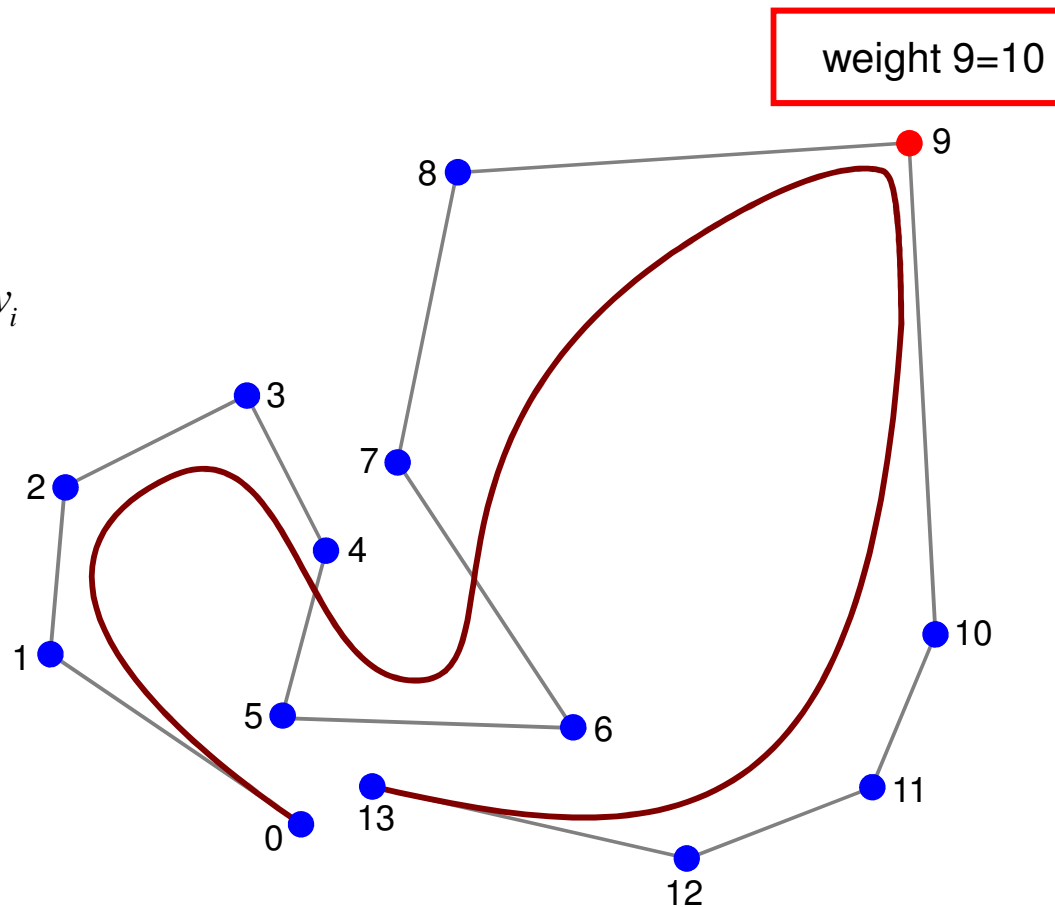
■ NURBS – Non-Uniform Rational B-splines

- weights at control points leads to more control over the shape of a curve
- projective transformation of a B-spline

$$R_i^p(\xi) = \frac{N_{i,p}(\xi) w_i}{W(\xi)}$$

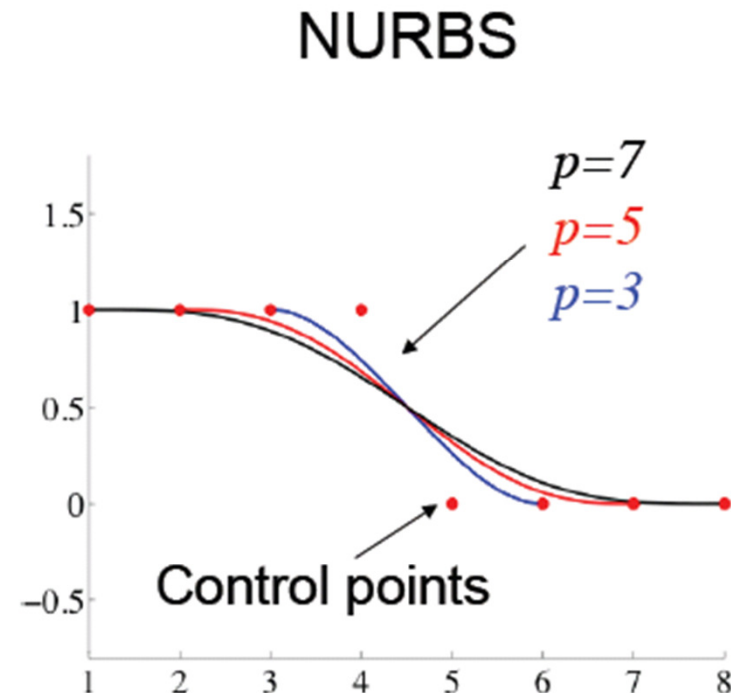
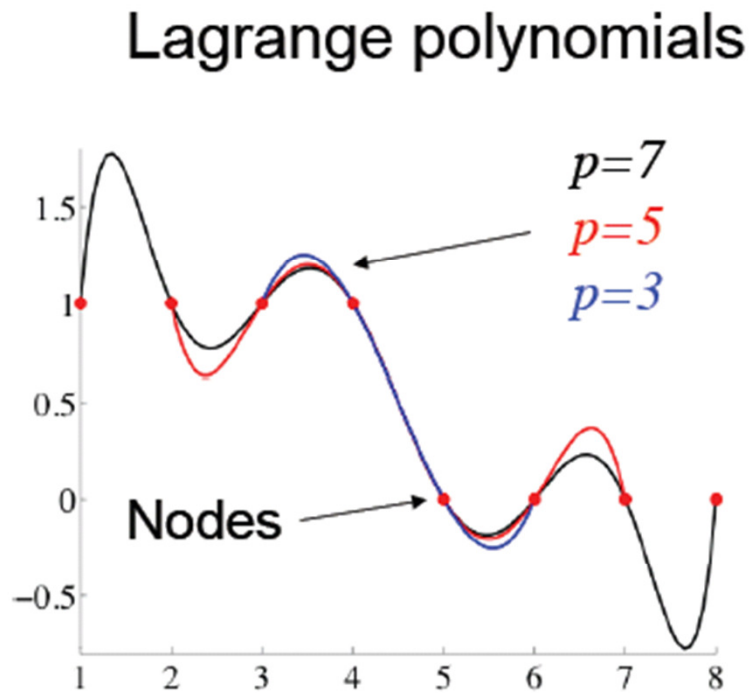
$$\text{with: } W(\xi) = \sum_{i=1}^n N_{i,p}(\xi) w_i$$

$$C(\xi) = \sum_{i=1}^n R_i^p(\xi) B_i$$



From B-splines to NURBS

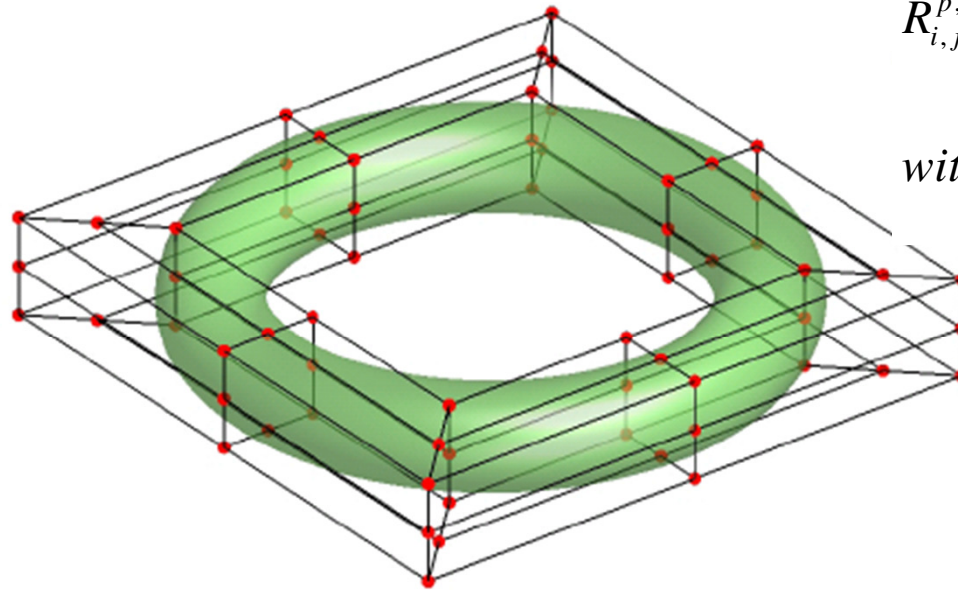
- smoothness of Lagrange polynomials vs. NURBS



T.J.R. Hughes

From B-splines to NURBS

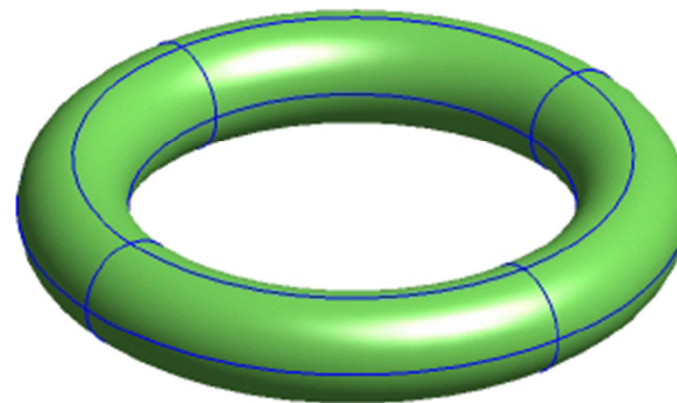
- NURBS – surfaces (tensor-product of univariate basis)



Control net

$$R_{i,j}^{p,q}(\xi, \eta) = \frac{N_{i,p}(\xi) M_{j,q}(\eta) w_{i,j}}{W(\xi, \eta)}$$

$$\text{with: } W(\xi, \eta) = \sum_{i=1}^n \sum_{j=1}^m N_{i,p}(\xi) M_{j,q}(\eta) w_{i,j}$$



Mesh

T.J.R. Hughes

From B-splines to NURBS - summary

■ B-spline basis functions

- recursive
- dependent on knot-vector and polynomial order
- normally $C^{(P-1)}$ -continuity
- „partition of unity“ (like Lagrange polynomials)
- refinement (h/p and k) without changing the initial geometry → adaptivity
- control points are normally not a part of the physical geometry (non-interpolatory basis functions)

■ NURBS

- B-spline basis functions + control net with weights
- all mentioned properties for B-splines apply for NURBS

generalized elements in LS-DYNA

- basis functions
 - active research as well in the field of CAD as in computer animation
- implementation of finite elements for specific basis functions
 - time consuming
 - software might become obsolete once new types of basis functions appear
- wish: possibility for fast prototyping of new elements



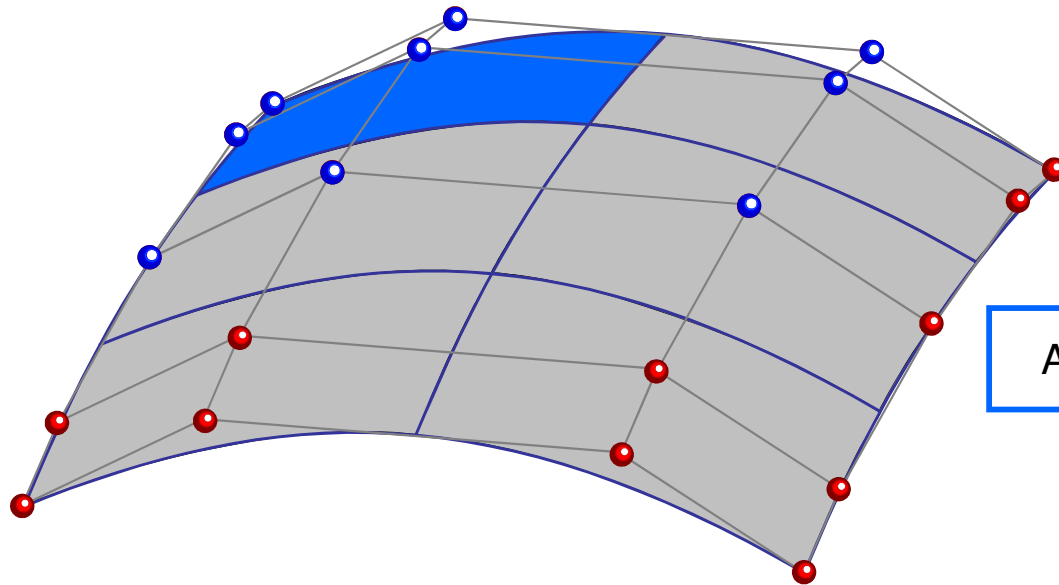
- ***generalized elements*** (***shells*** and ***solids***)
 - elements are formulated with the help of *generalized coordinates*
 - implementation is independent of utilized basis functions
 - new basis functions can be used immediately → rapid prototyping of elements
 - properties of *generalized elements* are defined exclusively in the input deck:
 - values of shape functions and its derivatives at generalized coordinates and integration points
 - values of integration weights
 - generalized formulation allows the use of different types of basis functions
 - Lagrange polynomials (standard FEA) / NURBS / T-splines / subdivision surfaces / ...

D.J. Benson

generalized elements in LS-DYNA - visualization

- generalized coordinates (coorespond to control points in NURBS)
 - are normally not part of the physical geometry
- LS-PrePost
 - displays only elements with linear basis functions
 - right now it is able to display and modify NURBS
- *interpolation elements*
 - linear elements to visualize results of generalized elements
 - are used for contact treatment
- *interpolation nodes*
 - nodes on physical geometry to define interpolation elements
 - displacements of interpolation nodes follow a linear function depending on displacements of generalized coordinates

generalized elements in LS-DYNA



*DEFINE_ELEMENT_GENERALIZED_SHELL
*ELEMENT_GENERALIZED_SHELL

Analysis

■ *DEFINE_ELEMENT_GENERALIZED_SHELL

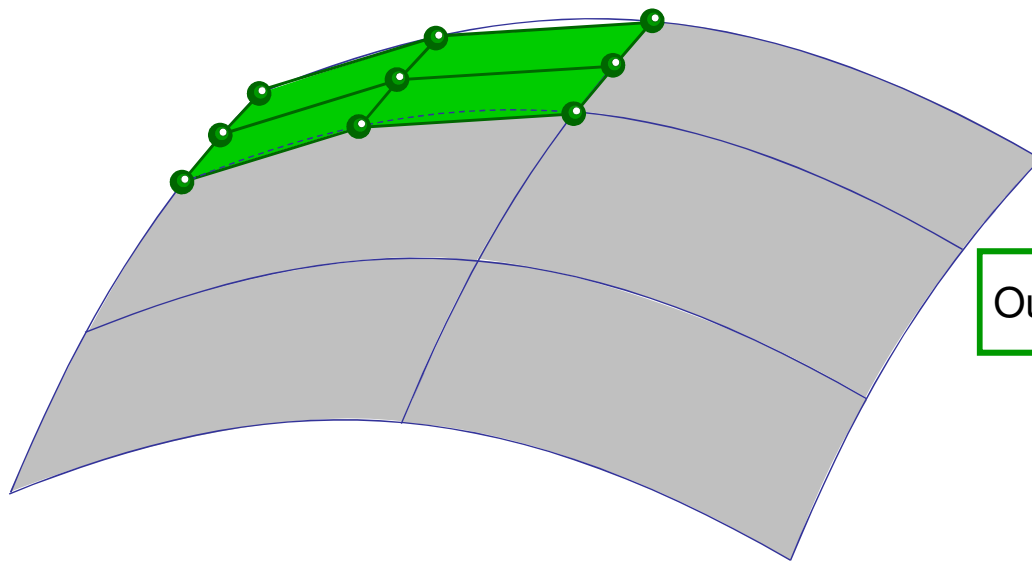
- element ID / number of IPs / number of generalized coordinates
- for each IP: weights & values of all basis functions and derivatives at IPs
- for each generalized coordinate: values of all basis functions and derivatives at control points

→ e.g.: a typical 9-noded element with 9 IPs necessitates approx. **172 lines** in input deck!

■ *ELEMENT_GENERALIZED_SHELL

- connectivity of an element (here: blue control points)

generalized elements in LS-DYNA



Output & BC

*CONSTRAINED_NODE_INTERPOLATION
*ELEMENT_INTERPOLATION_SHELL

- ***CONSTRAINED_NODE_INTERPOLATION**
 - for each interpolation node: number of control points of which the position of this interpolation node is dependent
 - IDs of control points and weighting factors
 - displacement of interpolation node will be interpolated linearly depending on the displacements of control points
 - will be used for contact treatment at the moment
- ***ELEMENT_INTERPOLATION_SHELL**
 - dependency to control points with appropriate weighting factors

generalized elements in LS-DYNA – shell formulations

■ shear deformable & thin shell theory

- with rotational DOFs
- without rotational DOFs

	shear deformable shell theory	thin shell theory
displacement field: $x(\eta, \xi, \zeta)$	$\sum_i N_i(\eta, \xi) \left(x_i + \frac{h}{2} \zeta \hat{y}_i \right)$	$\sum_i N_i(\eta, \xi) x_i + \frac{h}{2} \zeta \hat{n}(\eta, \xi)$
velocity field: $\dot{x}(\eta, \xi, \zeta)$	$\sum_i N_i(\eta, \xi) \left(\dot{x}_i + \frac{h}{2} \zeta \dot{\hat{y}}_i \right)$	$\sum_i N_i(\eta, \xi) \dot{x}_i + \frac{h}{2} \zeta \dot{\hat{n}}(\eta, \xi)$
unit orientation vector (shell normal):	\hat{y}	\hat{n}
time derivative of unit orientation vector:	with /without rotational DOFs $\dot{\hat{y}}_i = \boldsymbol{\omega}_i \times \hat{y}_i$ $\dot{\hat{y}}_i = \sum_j \frac{\partial \hat{y}_i}{\partial x_j} \dot{x}_j$	with / without rotational DOFs

generalized elements in LS-DYNA

- analysis capabilities
 - implicate and explicit time integration
 - eigenvalue analysis
 - many material models from the LS-DYNA material library are available

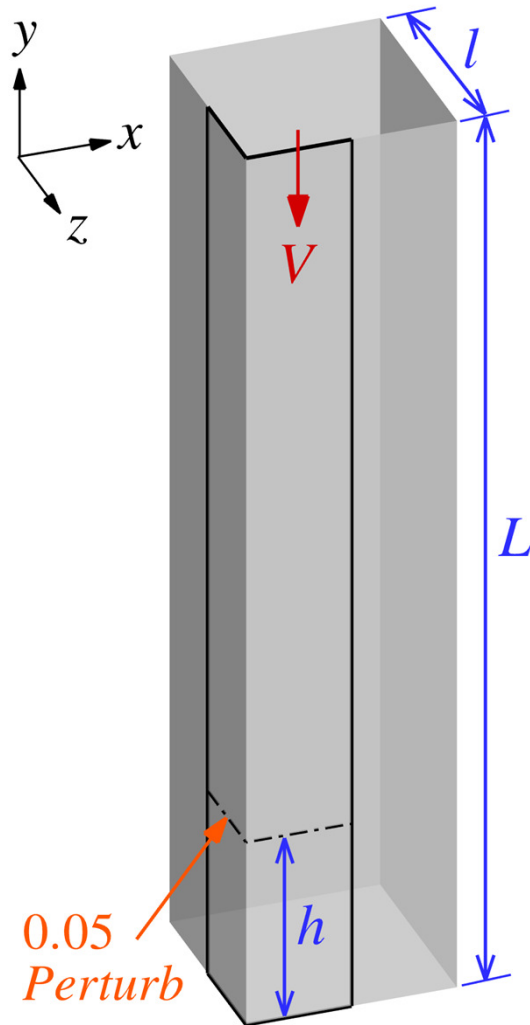
- some boundary conditions are implemented via *interpolation elements*
 - contact treatment
 - pressure distribution (not fully tested yet)

- time step control via „*maximum system eigenvalue*“
 - D.J. Benson: *Stable Time Step Estimation for Multi-material Eulerian Hydrocodes*, CMAME, 191-205 (1998)

- generalized **solids** are implemented as well
 - „standard“ displacement elements

generalized elements in LS-DYNA - Example

■ buckling of a square tube (using NURBS basis functions)



- standard benchmark for automobile crashworthiness
- quarter symmetry to reduce cost
- perturbation to initiate buckling mode
- J_2 plasticity with linear isotropic hardening
- mesh:
 - 640 quartic ($P=4$) elements.
 - 1156 control points.
 - 3 integration points through thickness.

D.J. Benson

- buckling of a square tube (NURBS-elements: $p=4$)

square cross section for single surface

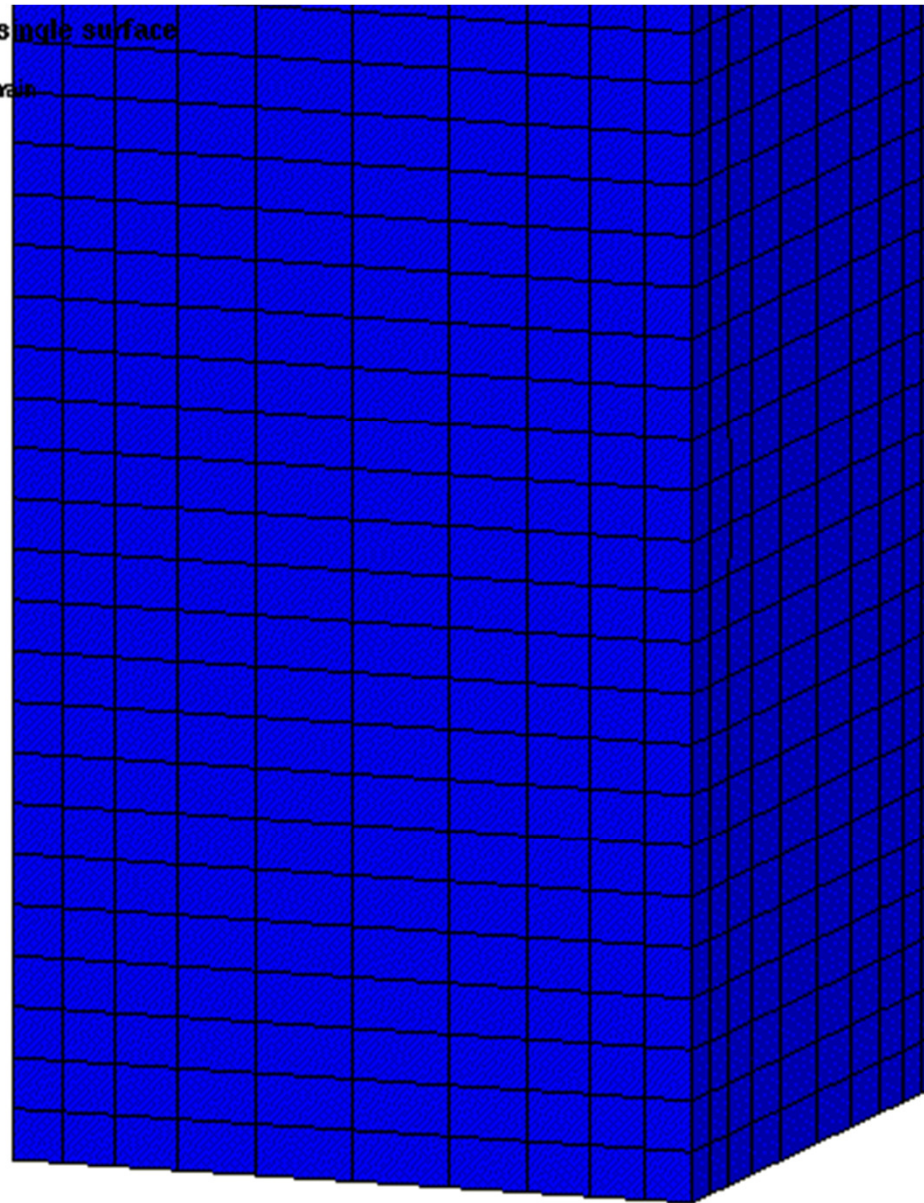
Time = 0

Contours of Effective Plastic Strain

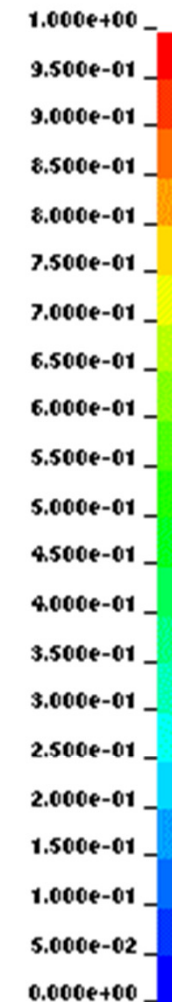
max ip1 value

min=0, at elem# 1001

max=0, at elem# 1001

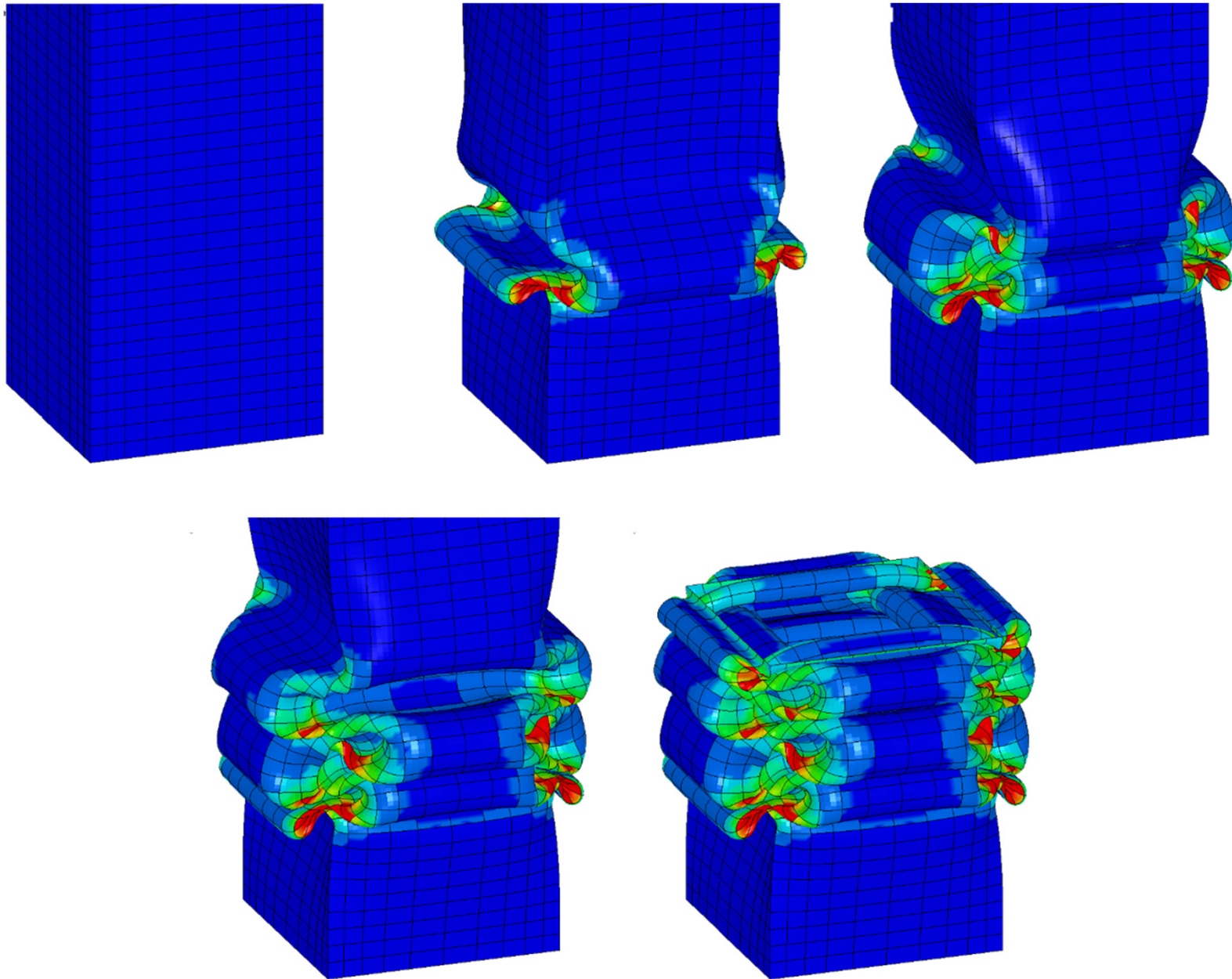


Fringe Levels



D.J. Benson

- buckling of a square tube (NURBS-elements: $p=4$)

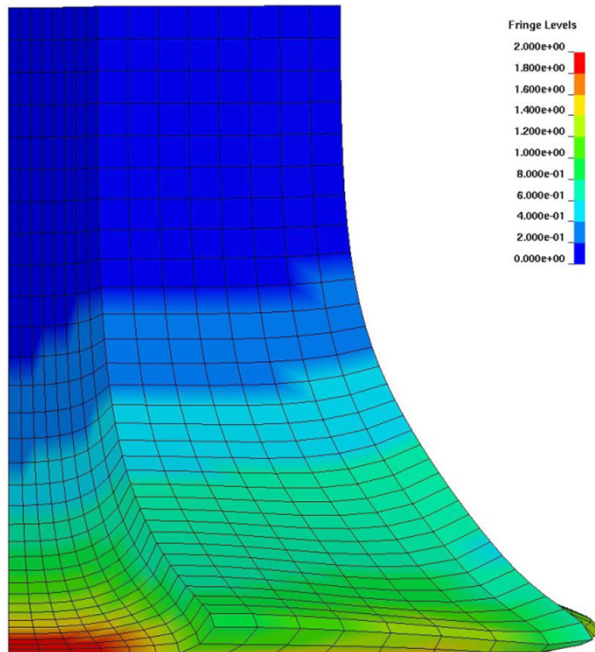


D.J. Benson

generalized elements in LS-DYNA – solid elements

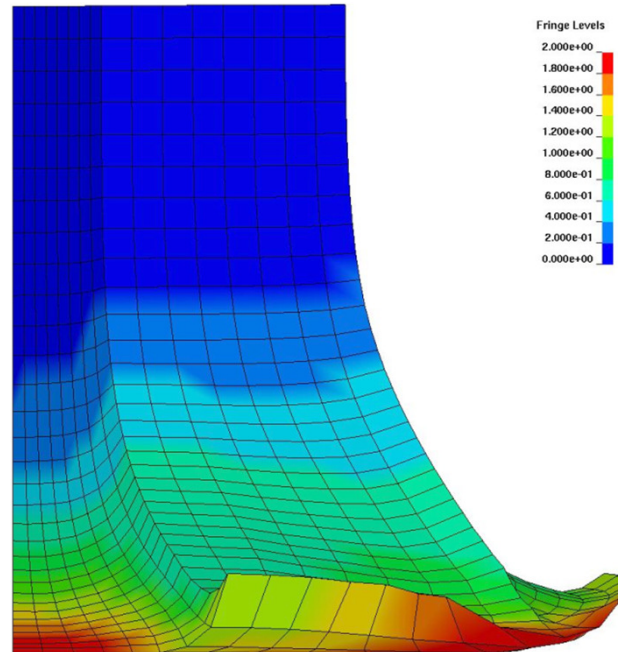
■ Taylor Bar Impact

1-Pnt Hex



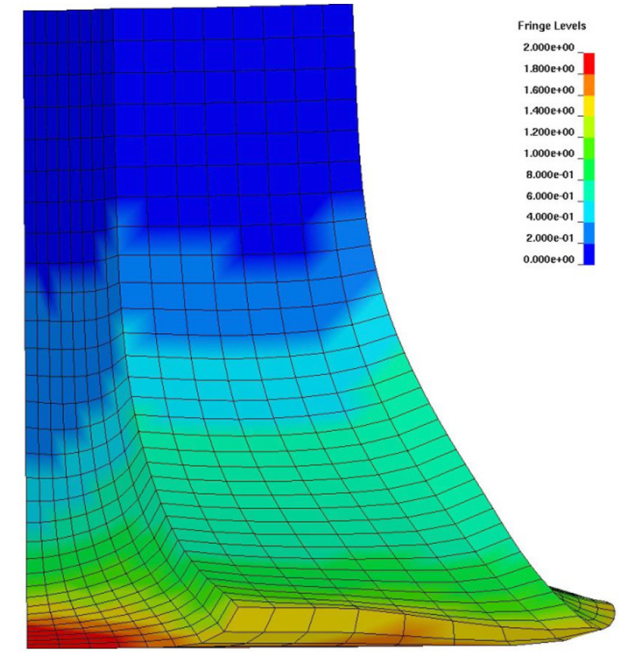
Standard LS-DYNA element

27 Node Quadratic



Generalized Element

Quadratic NURBS



Generalized Element

Formulation	# Nodes/ CP	Peak Plastic Strain	# Time Steps
1-Pnt Hex	2677	2.164	2136
Quad. Lagr.	2677	2.346	3370
Quad. NURBS	648	2.479	954

D.J. Benson

generalized elements in LS-DYNA - summary

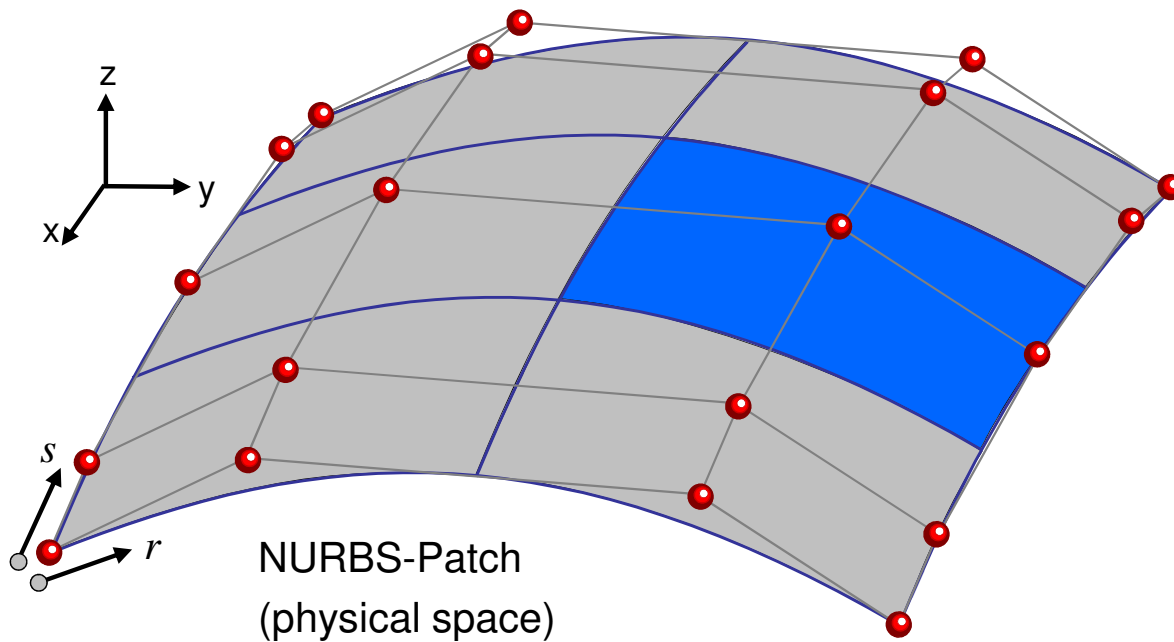
- fast prototyping of new elements
 - all the information in the input deck
 - no limitation on number of control points and integration points per element
 - no restriction to special types of basis functions
 - interesting for research
 - rather difficult to create input deck → not usable for industry
 - good results with NURBS → decision to implement NURBS-based finite elements in LS-DYNA

- generalized shells
 - shear deformable and thin shell theories implemented
 - with and without rotational DOFs

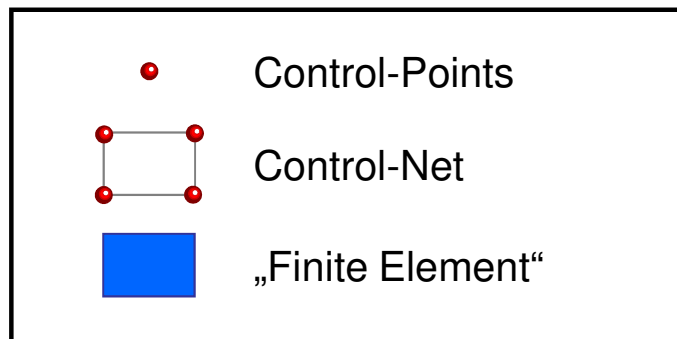
- generalized solids
 - „standard“ displacement formulation

NURBS-based finite elements in LS-DYNA

- A typical NURBS-Patch and the definition of elements
 - elements are defined through the knot-vectors (interval between different values)
 - shape functions for each control-point



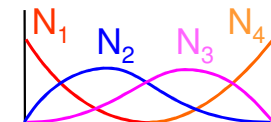
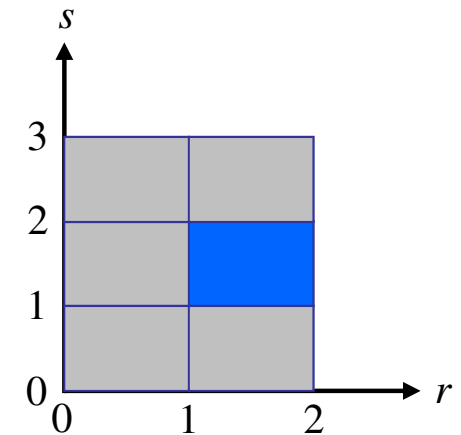
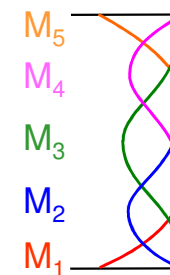
NURBS-Patch
(physical space)



polynomial order:

- quadratic in r-direction ($p_r=2$)
- quadratic in s-direction ($p_s=2$)

sknot=[0,0,0,1,2,3,3,3]



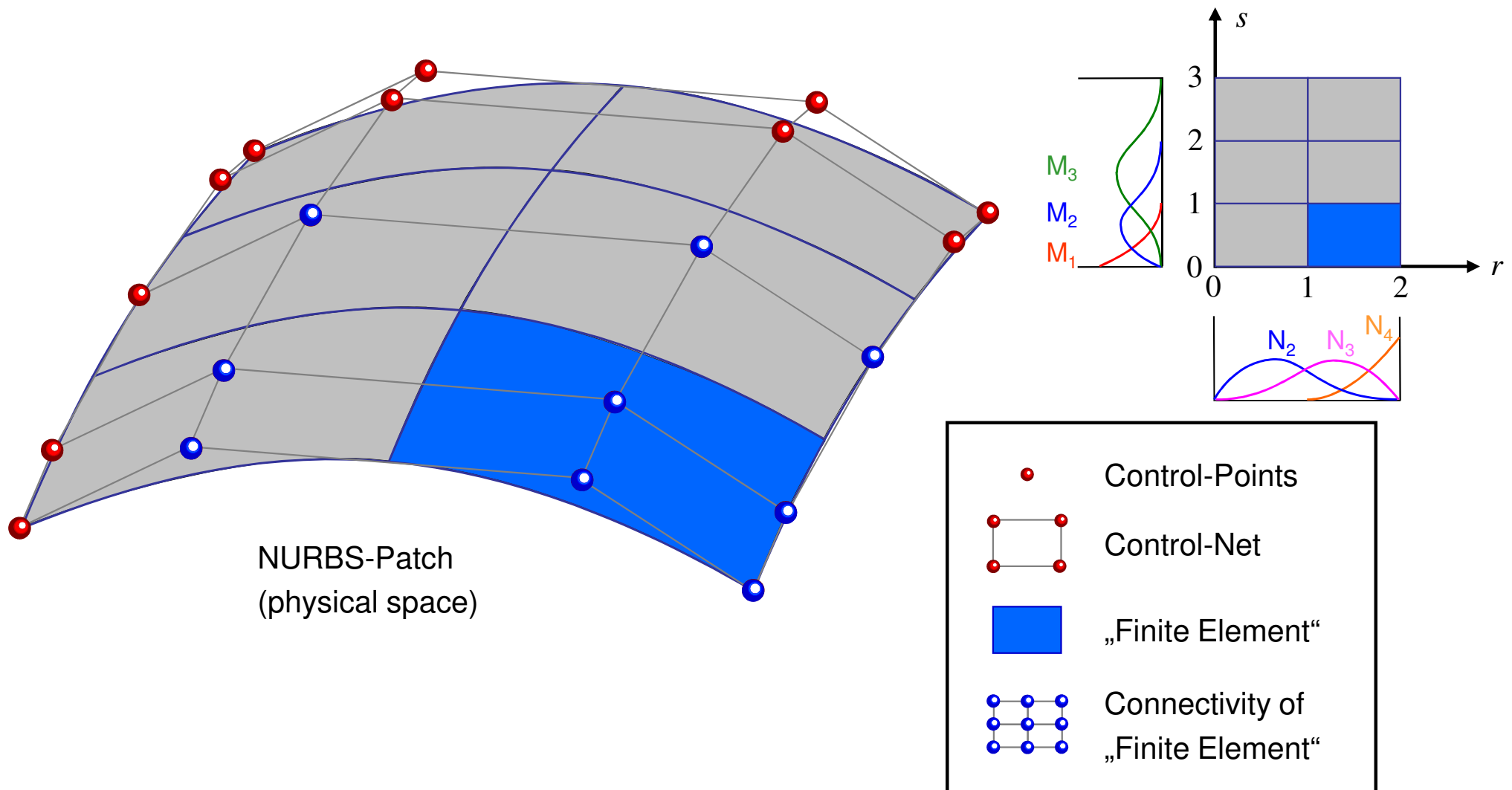
NURBS-Patch
(parameter space)

rknot=[0,0,0,1,2,2,2,2]

NURBS-based finite elements in LS-DYNA

■ A typical NURBS-Patch – Connectivity of elements

- Possible „overlaps“ (→ higher continuity!)
- Size of „overlap“ depends on polynomial order (and on knot-vector)



NURBS-based finite elements in LS-DYNA

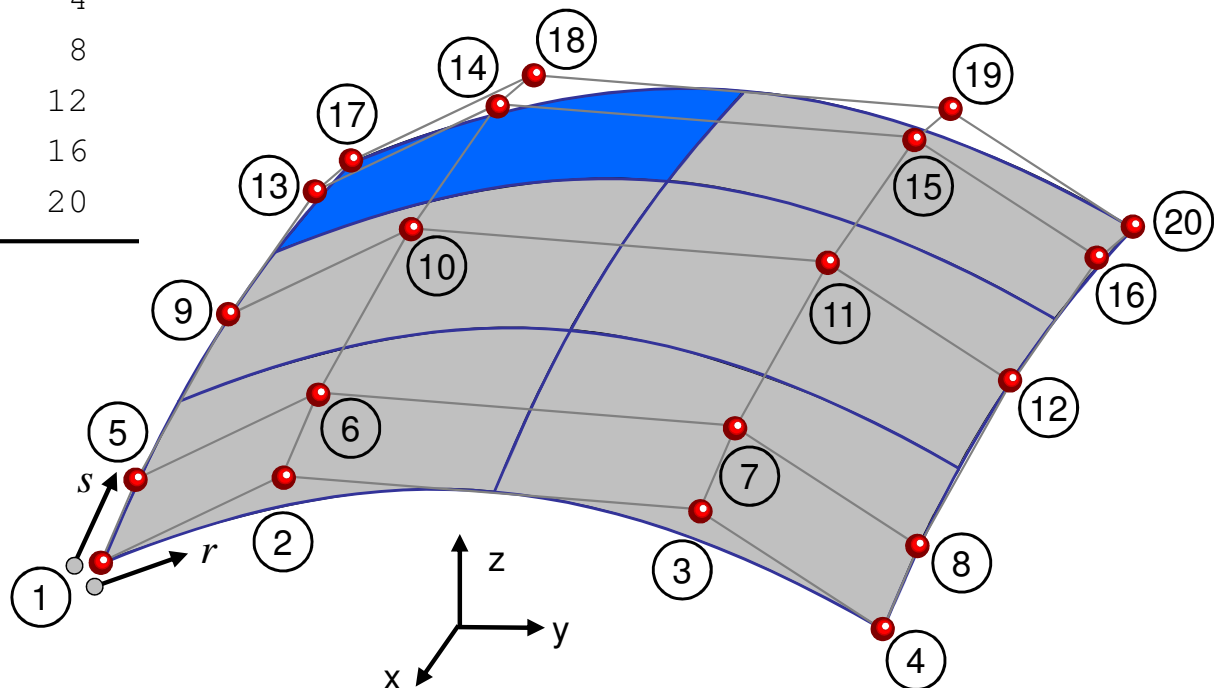
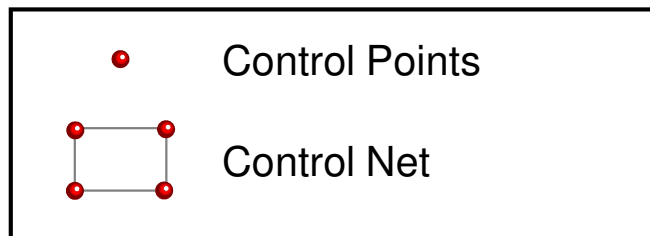
- New Keyword: *ELEMENT_NURBS_PATCH_2D
 - definition of NURBS-surfaces
 - 4 different shell formulations with/without rotational DOFs (→ generalized shells)
- Pre- and Postprocessing
 - work in progress for LS-PrePost ... current status (lspp3.1beta)
 - visualization of 2D-NURBS-Patches
 - import IGES-format and construct *ELEMENT_NURBS_PATCH_2D
 - modification of 2D-NURBS geometry
 - ... much more to come!
- Postprocessing and boundary conditions (i.e. contact) currently with
 - interpolation nodes
 - interpolation elements
- Analysis capabilities (→ generalized shells)
 - implicit and explicit time integration
 - eigenvalue analysis
 - other capabilities (e.g. geometric stiffness for buckling) implemented but not yet tested
- LS-DYNA material library available (including umats)

NURBS-based finite elements in LS-DYNA



*ELEMENT_NURBS_PATCH_2D

\$----	EID-----	PID-----	NPR-----	PR-----	NPS-----	PS-----	7-----	8-----
	11	12	4	2	5	2		
\$----	WFL-----	FORM-----	INT-----	NISR-----	NISS-----	IMASS-----	7-----	8-----
	0	0	1	2	2	0		
\$rk+	1-----	2-----	3-----	4-----	5-----	6-----	7-----	8-----
	0.0	0.0	0.0	1.0	2.0	2.0	2.0	
\$sk+	1-----	2-----	3-----	4-----	5-----	6-----	7-----	8-----
	0.0	0.0	0.0	1.0	2.0	3.0	3.0	3.0
\$net+	N1-----	N2-----	N3-----	N4-----	N5-----	N6-----	N7-----	N8-----
	1	2	3	4				
	5	6	7	8				
	9	10	11	12				
	13	14	15	16				
	17	18	19	20				



NURBS-based finite elements in LS-DYNA



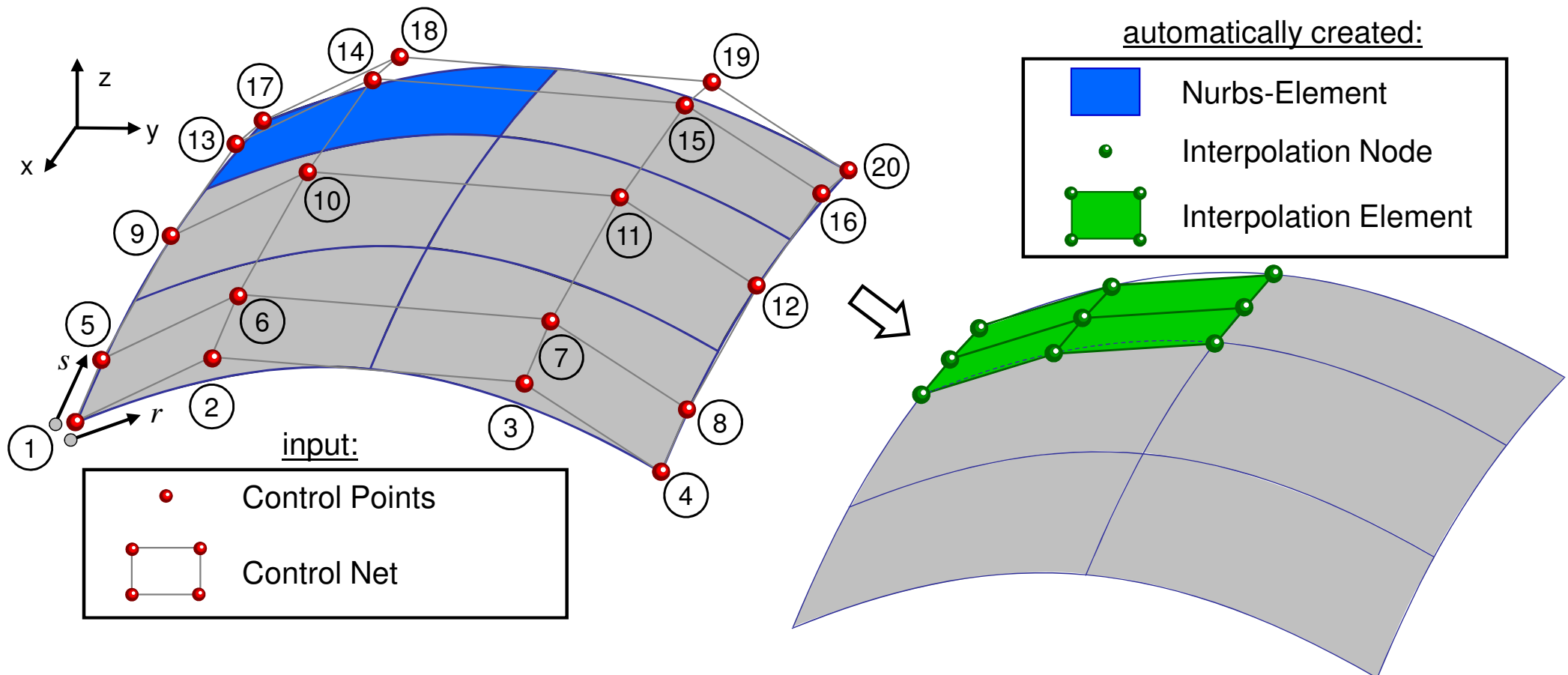
```
...  
$---+--WFL-----+--FORM-----+--INT-----+--NISR-----+--NISS-----+IMASS  
          0           0           1           2           2           0
```

- **WFL** – Flag for weighting factors for control points
 - 0: All weights are 1.0 (no need to define them → B-splines)
 - 1: define weights for control points
- **FORM** – Shell formulation to be used
 - 0: “shear deformable theory” with rotational DOFs
 - 1: “shear deformable theory” without rotational DOFs
 - 2: “thin shell theory” without rotational DOFs
 - 3: “thin shell theory” with rotational DOFs
- **INT** – In-plane integration rule
 - 0: reduced (Gauss-)integration ($NIP=PR*PS$)
 - 1: full (Gauss-)integration ($NIP=(PR+1)*(PS+1)$)
 - ?: “Half-Point-Rule” (→ A. Reali)

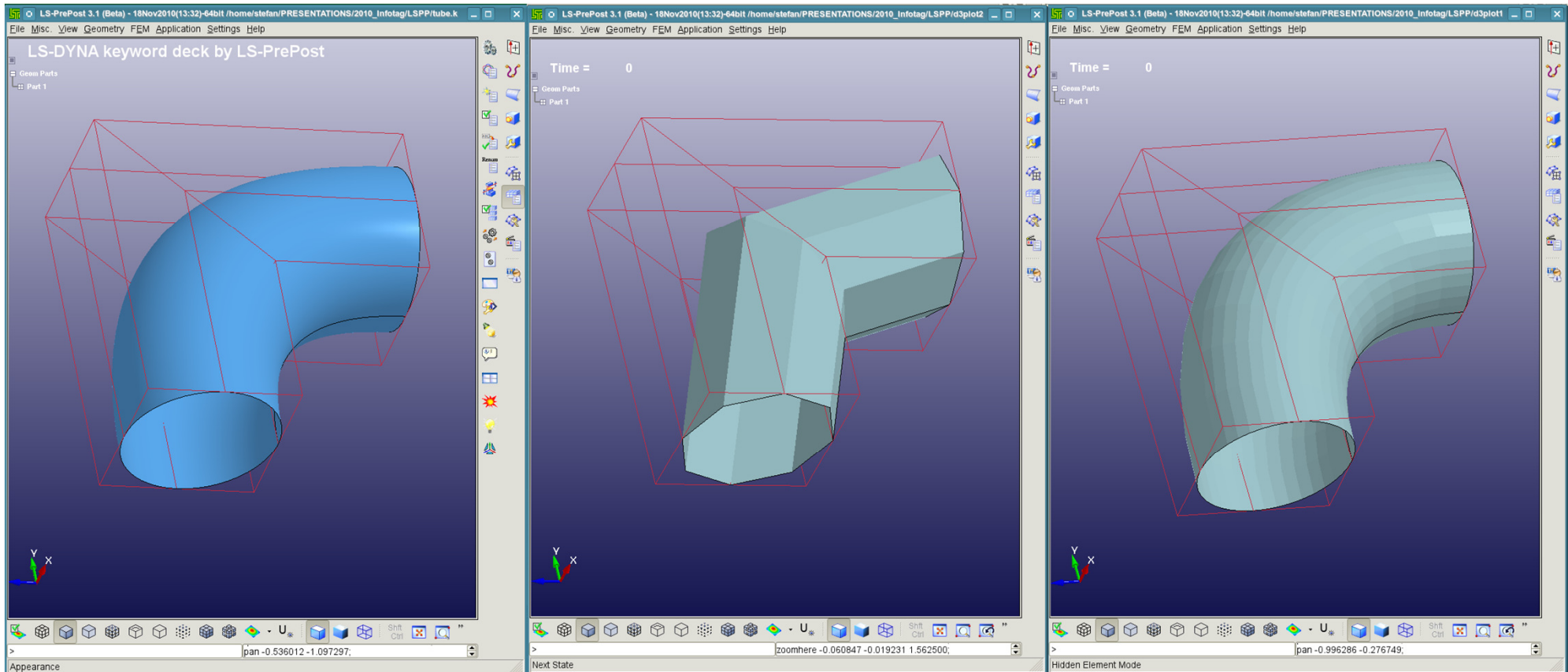
NURBS-based finite elements in LS-DYNA

```
...  
$---+--WFL-----+--FORM-----+--INT-----+--NISR-----+--NISS-----+IMASS  
          0           0           1           2           2           0
```

- **NISR/NISS** – Number of Interpolation Elements per Nurbs-Element (r-/s-dir.)
important for post-processing, boundary conditions and contact treatment



NURBS-based finite elements in LS-DYNA



LSPP: Preprocessing

- control-net
- nurbs surface

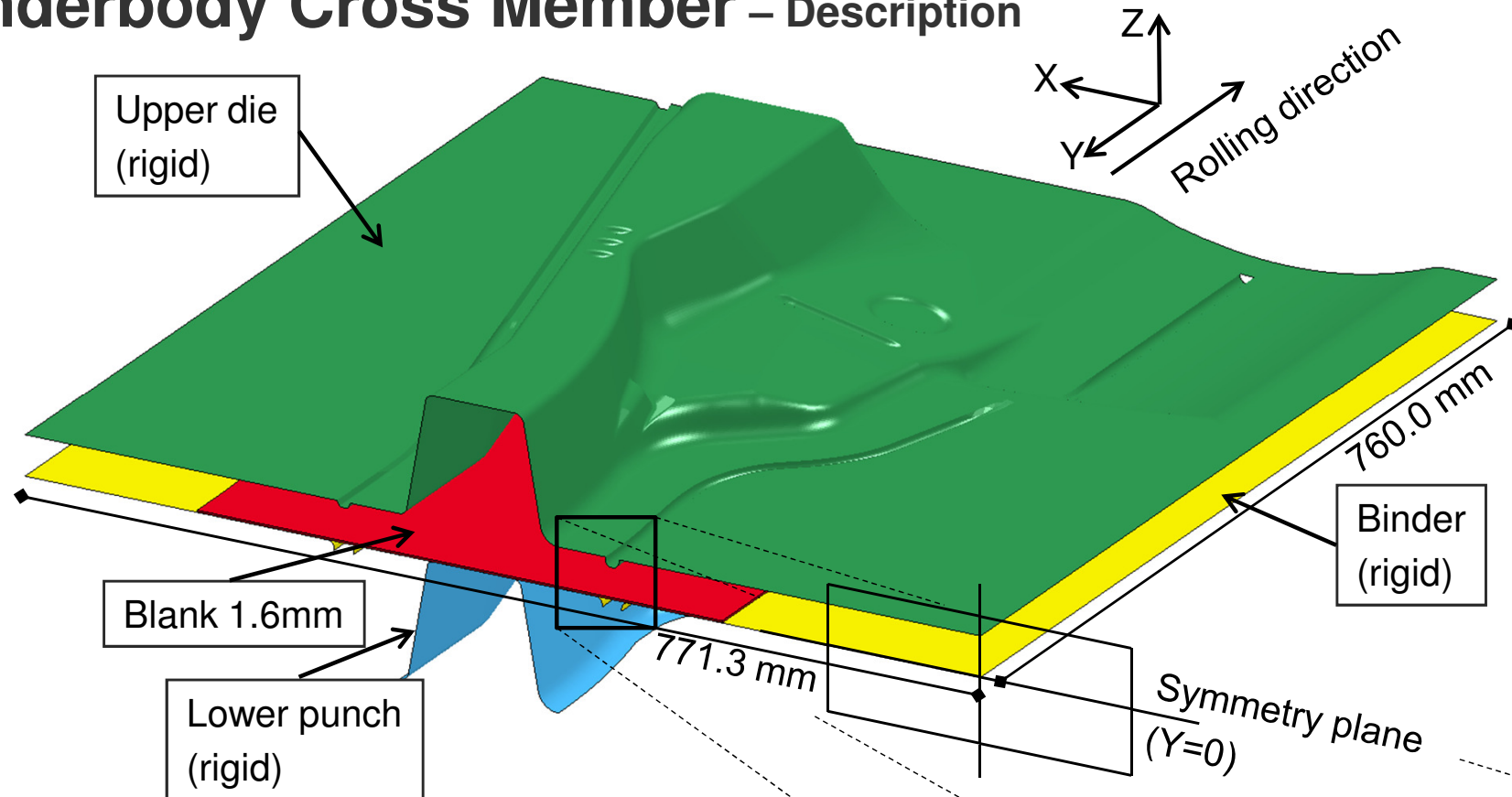
nistr=niss=2

LSPP: Postprocessing

- Interpolation nodes/elements

nistr=niss=10

Underbody Cross Member – Description



■ Tool moving directions

- Lower punch: stationary
- Upper die: moving (z-direction)
- Binder: moving (z-direction – travel: 100mm)

■ Blank-Material

- AL5182-O (Aluminium)

Underbody Cross Member – Simulation models

■ identical for all

- material model: *MAT_TRANSVERSELY_ANISOTROPIC_ELASTIC_PLASTIC (*MAT_037)
- nip=5 number of integration points through the thickness
- istupd=0 no thickness update
- imsc1=0 no “selective” mass scaling (no mass scaling at all!)
- SMP, double precision, ncpu=4 (Dual Core AMD Opteron, 2.2 GHz)

■ standard elements

- ELFORM=16: fully integrated (4-noded) shell-elements with assumed strain formulation
- discretizations: with adaptivity (mesh size: 4mm → 2mm → 1mm) as reference solution
 without adaptivity: mesh-sizes: 2mm; 4mm; 8mm

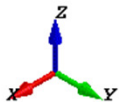
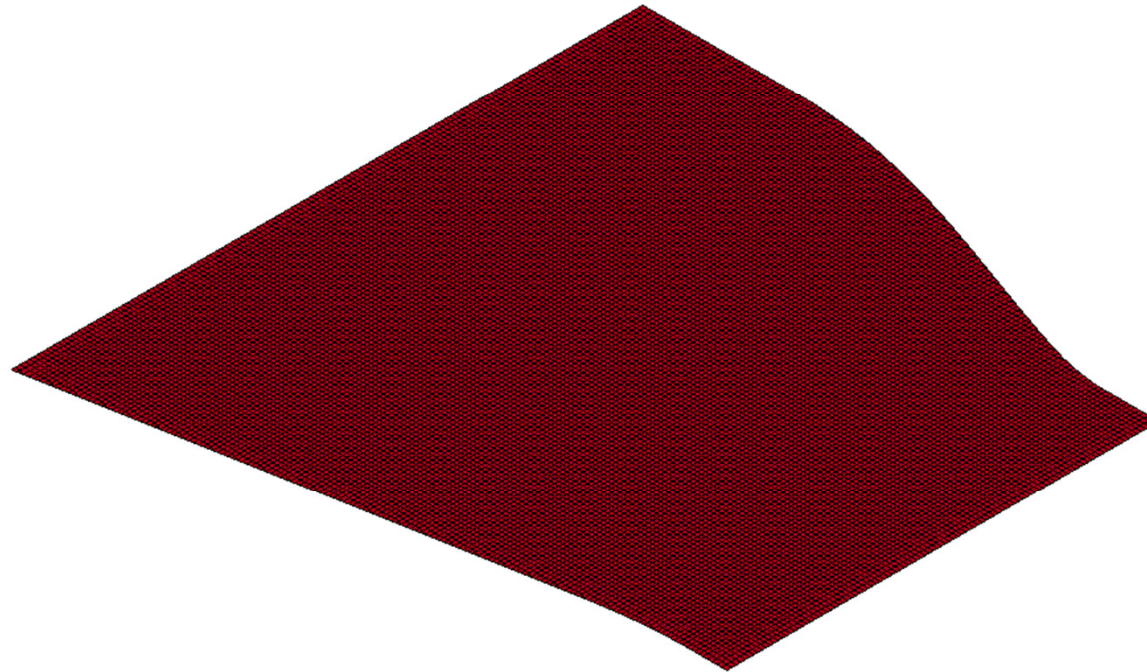
■ 2D-NURBS elements

- Formulation: FORM=2 (rotation free formulation)
- Integraion rule: INT=0 (reduced integration)
- Polynomial: p2 (quadratic), p3 (cubic), p4 (quartic), p5 (quintic)
- discretizations: mesh-sizes: 4mm; 8mm; 16mm
- number of interpolation elements/ NURBS-elements: NISR=PR; NISS=PS

Underbody Cross Member – Standard-Elements

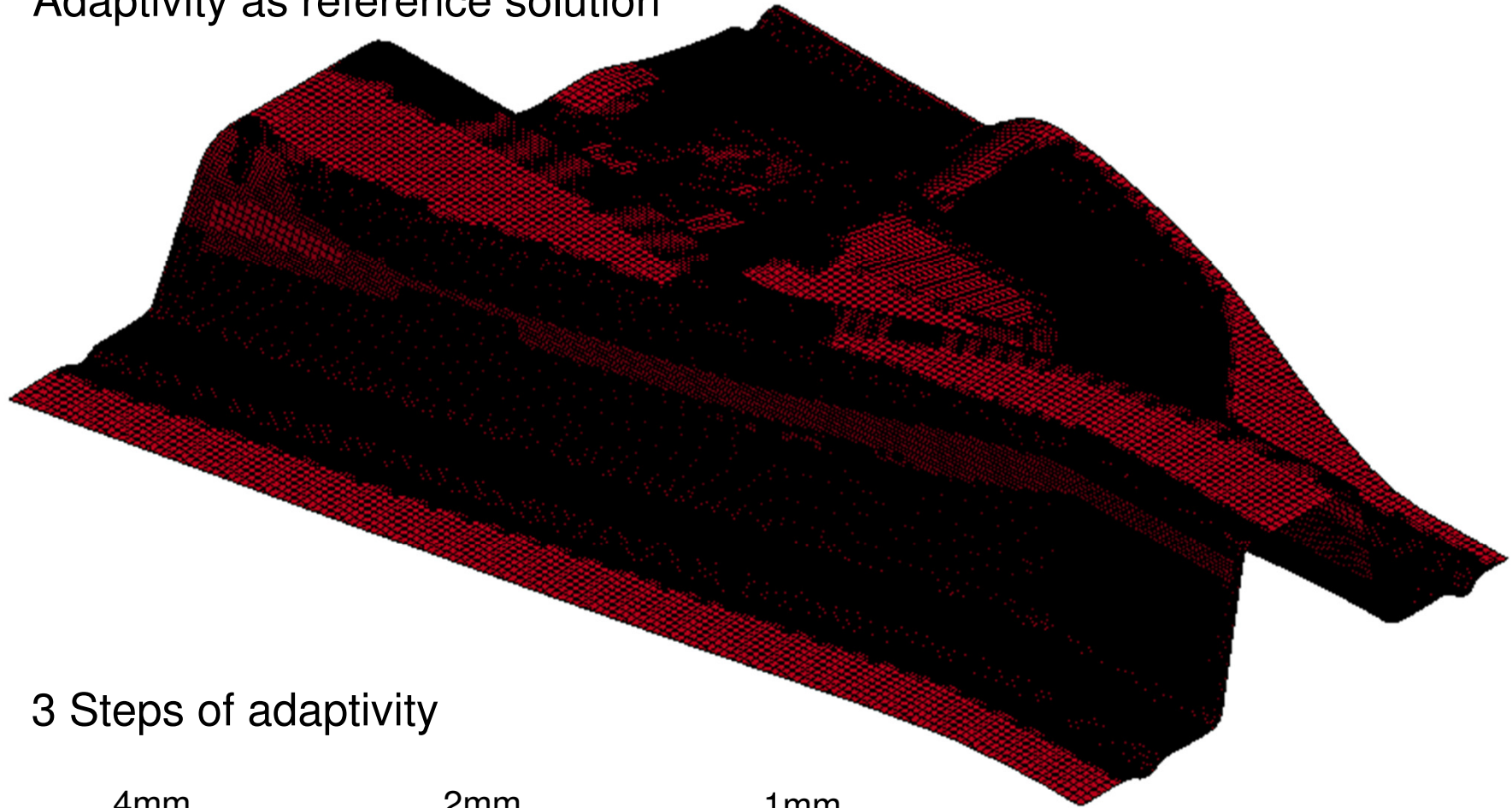
- Adaptivity as reference solution

Numisheet2005-BM2 - DL-Adaptiv (4mm ->
Time = 0, #nodes=85814, #elem=88980

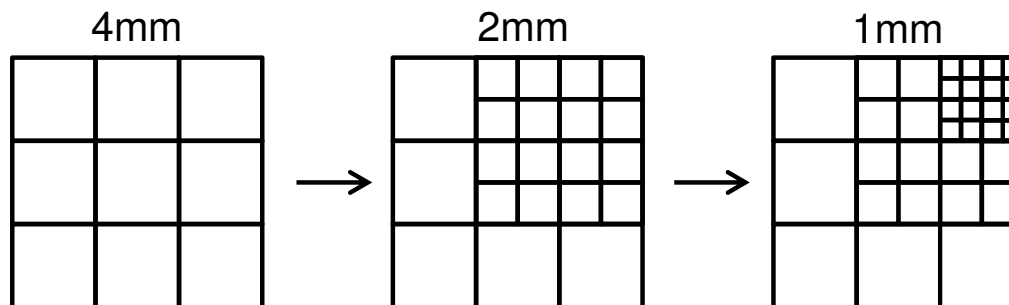


Underbody Cross Member – Standard-Elements

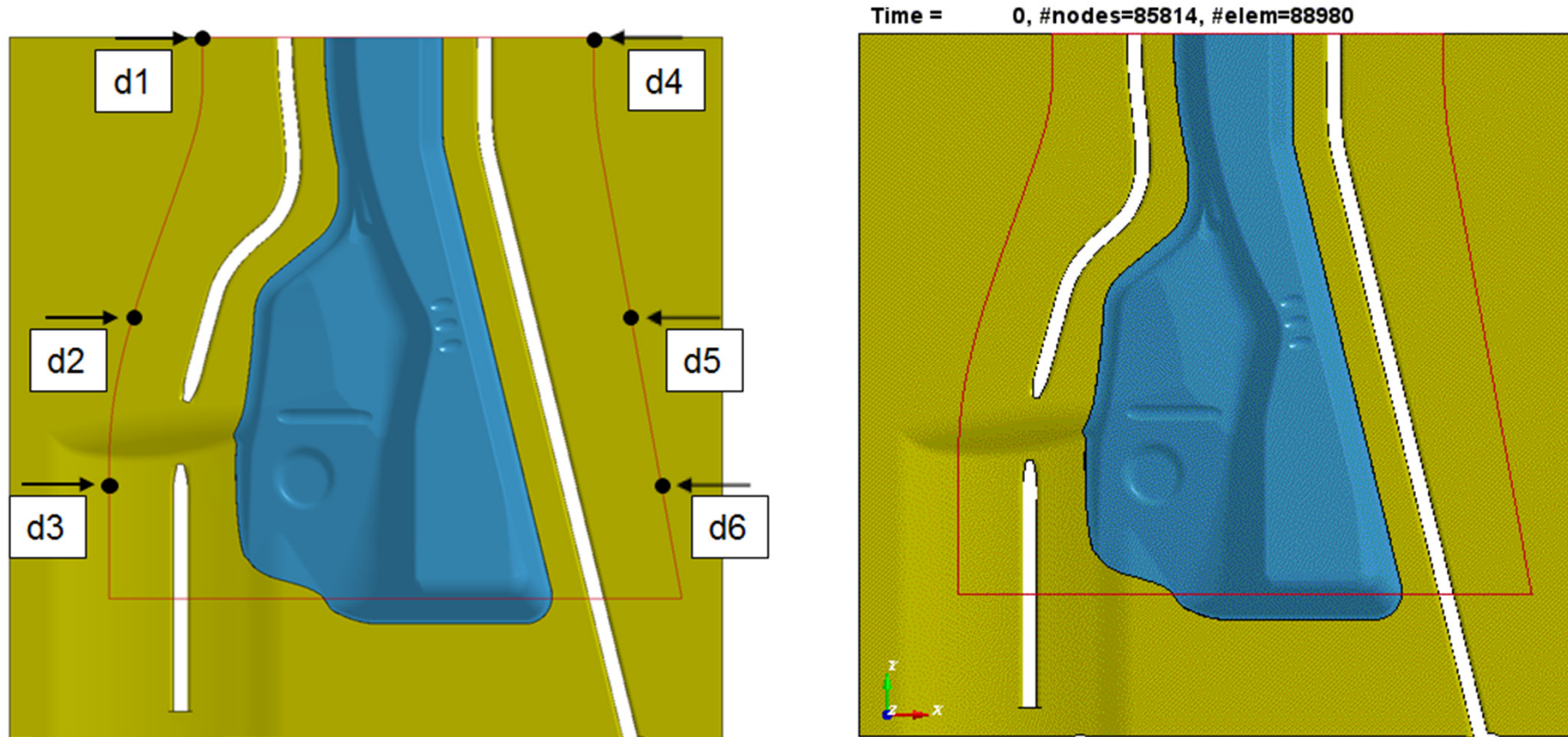
- Adaptivity as reference solution



- 3 Steps of adaptivity



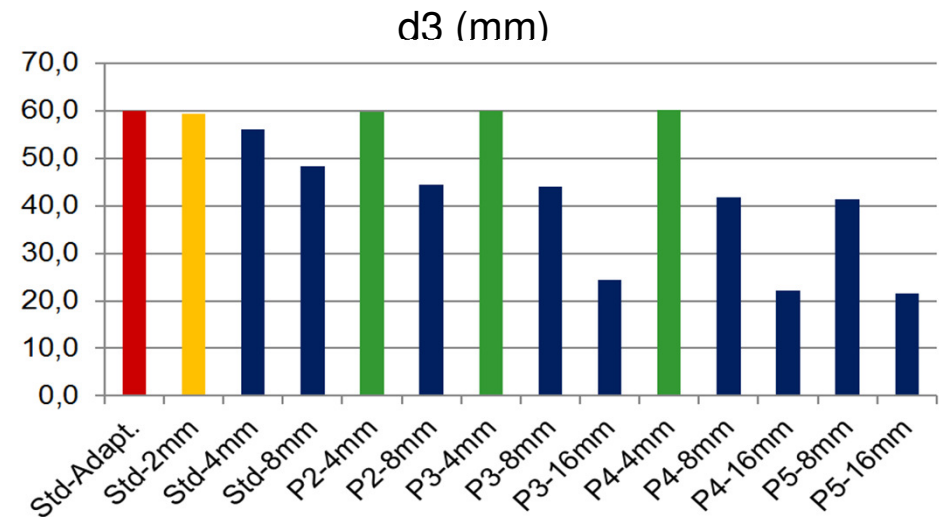
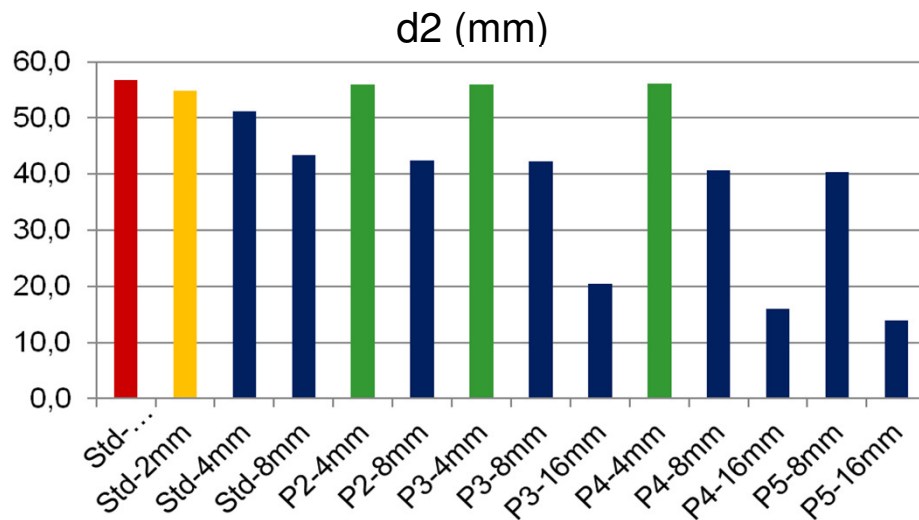
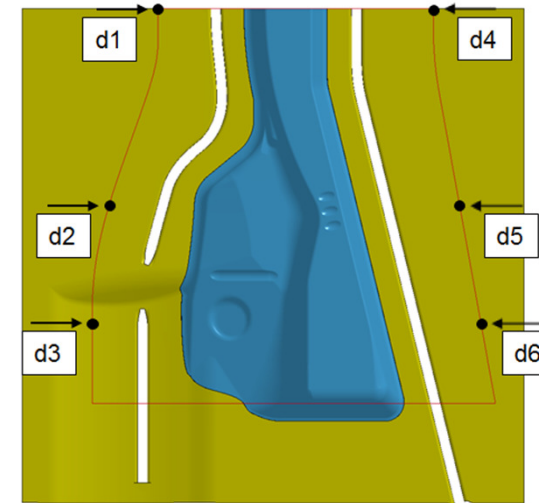
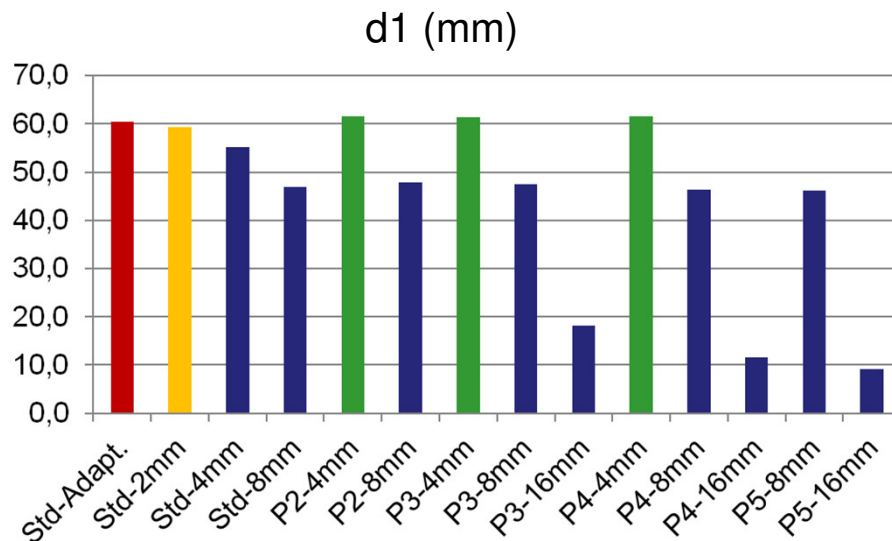
Underbody Cross Member – Draw-in



■ Results → Use “Adaptiv” as reference solution

	d1(mm)	d2(mm)	d3(mm)	d4(mm)	d5(5mm)	d6(6mm)
Benchmark	62.2	51.8	56.0	73.7	57.6	47.8
Adaptiv	60.5	56.8	59.9	74.8	57.5	50.4

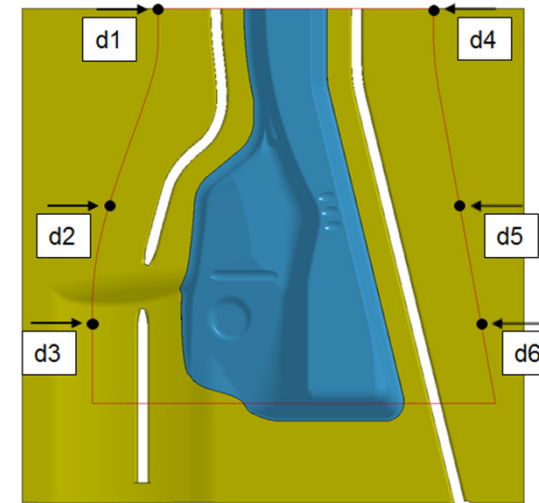
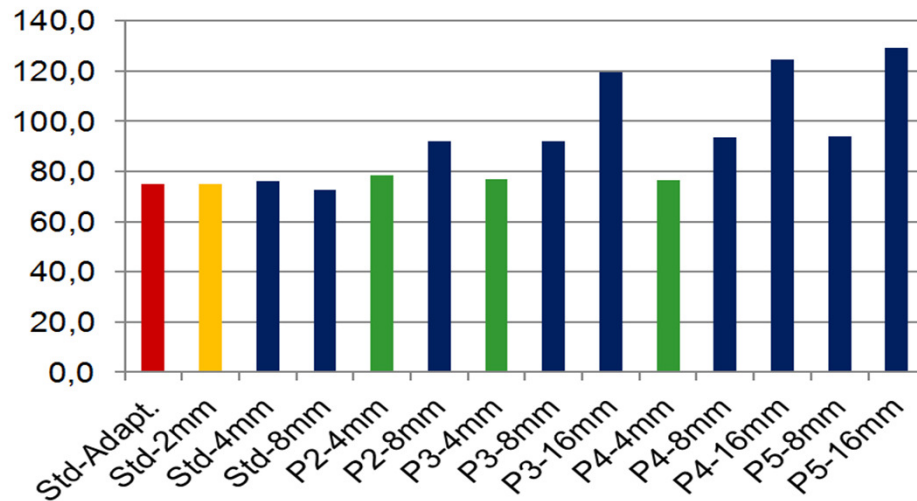
Underbody Cross Member – Draw-in



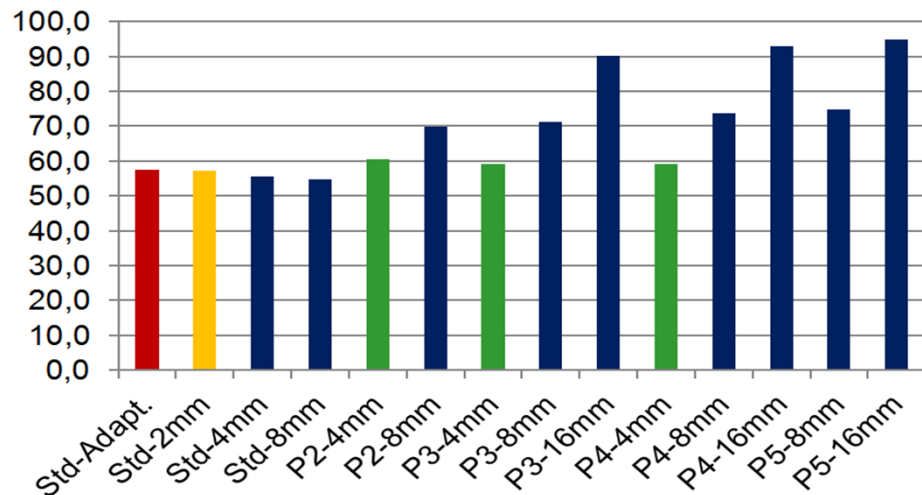
■ larger mesh size → less draw-in (behavior is too stiff)

Underbody Cross Member – Draw-in

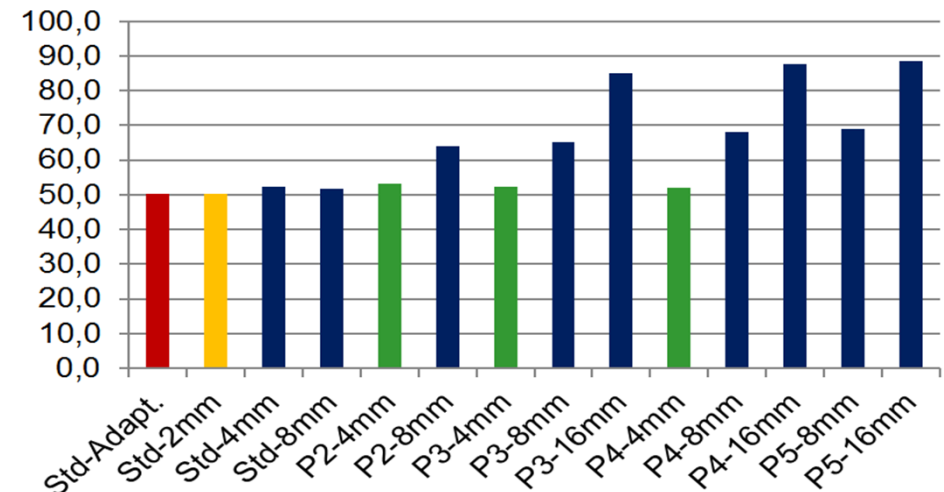
d4 (mm)



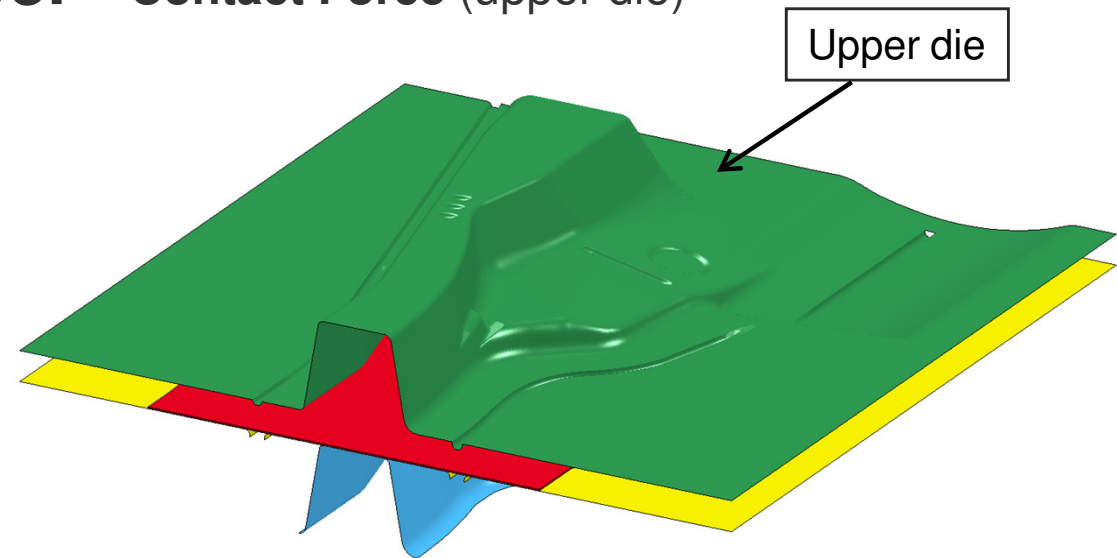
d5 (mm)



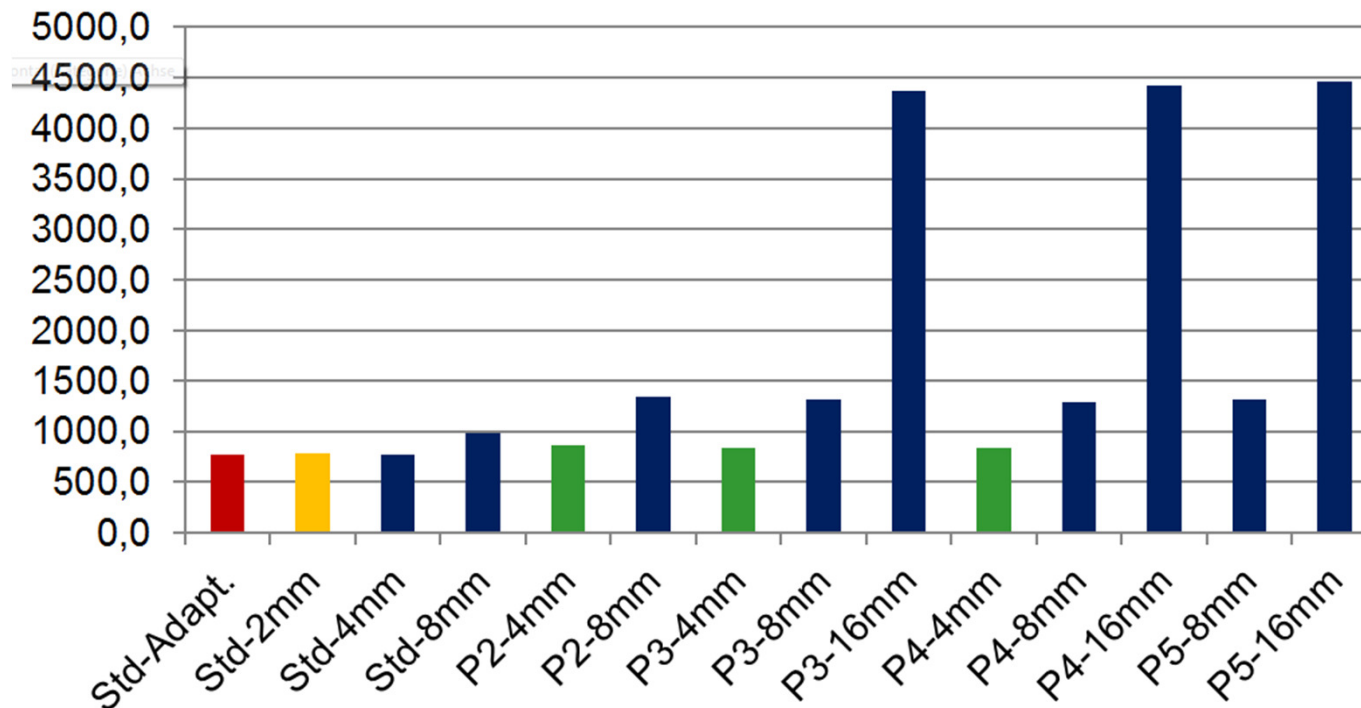
d6 (mm)



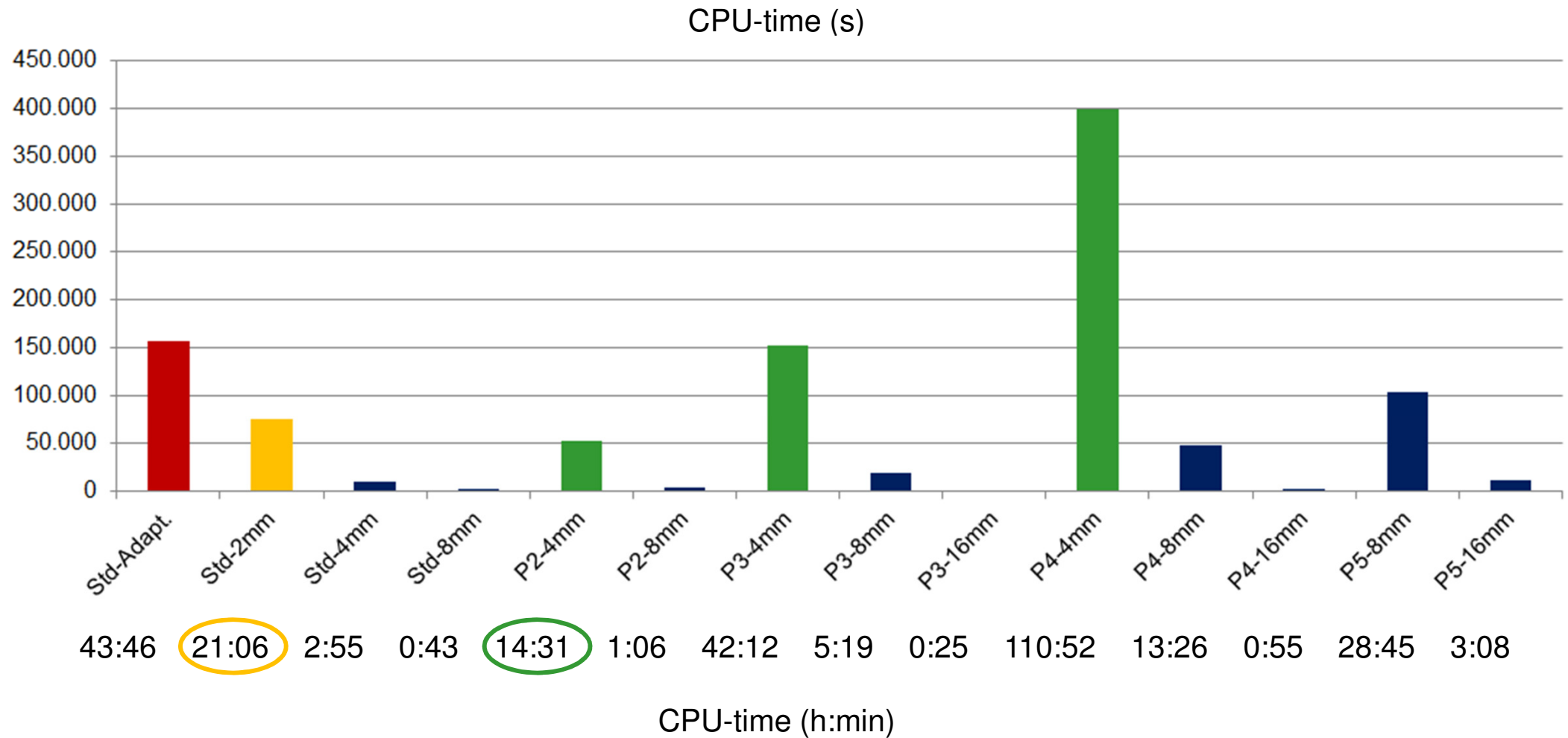
Underbody Cross Member – Contact Force (upper die)



Contact Force (kN)

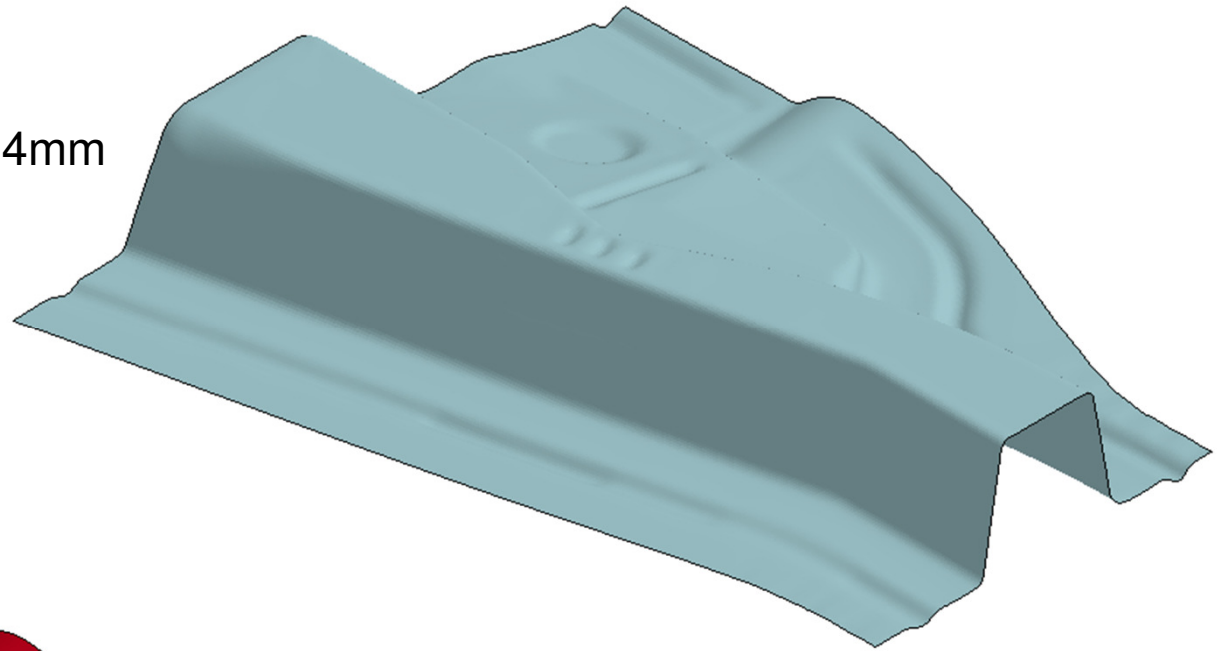


Underbody Cross Member – CPU-time

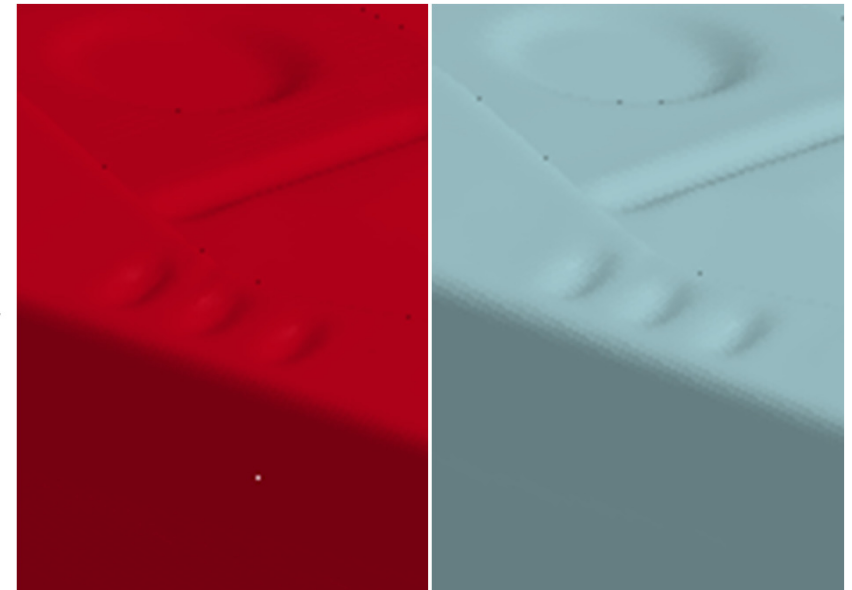
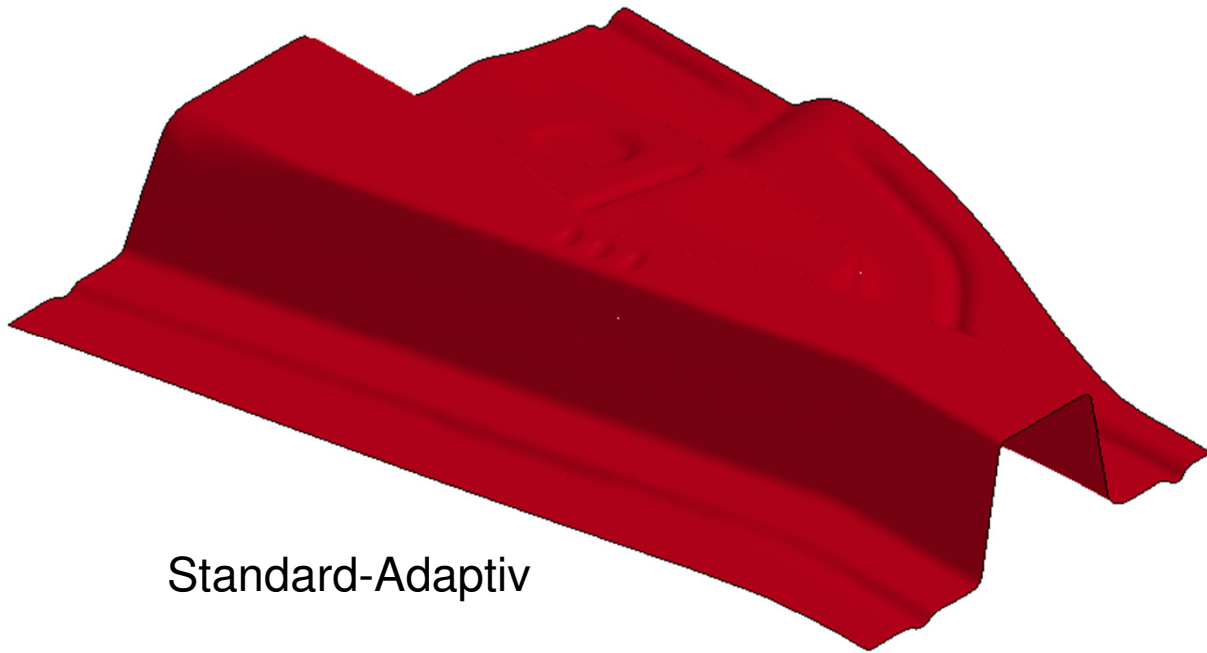


Underbody Cross Member – Final deformation

NURBS-P2-4mm

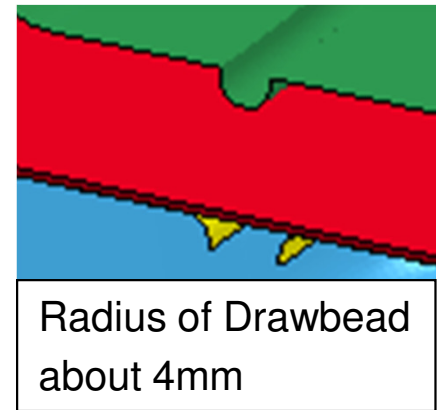


Standard-Adaptiv



Underbody Cross Member – Summary

- Detailed discretization of “Drawbead” needs a fine discretization ($\leq 4\text{mm}$), no matter what type of elements
- Rotation free elements with reduced integration show best behavior
- CPU-time for comparable discretizations (i.e: $p1_2\text{mm} \leftrightarrow p2_4\text{mm}$) are promising (no CODE optimization yet!) \rightarrow cost competitive
- CPU-time increase for NURBS with same discretizations for next order of polynomial (i.e.: $p2_4\text{mm} \rightarrow p3_4\text{mm}$): Factor 2.5-2.8
- Higher order does not help anything in this example (spacing of control points define mesh size)



Summary

- NURBS-based elements run stable
- higher order accurate isogeometric analysis can be cost competitive
 - but missing a couple of “special” issues for industrial sheet metal forming applications
- code optimization necessary to make it faster
- in this example: geometry dictates the mesh size (independent of polynomial order!)

Outlook

- perform a lot more studies in different fields → experience
- motivate customers (and **researchers**) to “play” with these elements
- further implementation
 - make NURBS elements work with MPP
 - (selective) mass scaling
 - thickness update of shells
 - use NURBS for contact (instead of interpolation elements)
 - make pre- and post-processing more user-friendly
 - introduce 3D NURBS elements
 - ... much more

Thank you!

